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Chris Smith & Associates

Proposed Residential Development -Toolamba

Traffic Impact Assessment

July 2015

<u>Report</u>

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- C Traffic Counts
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- E VLimits Report

1. Introduction

Paffrath Consulting has been engaged by Chris Smith & Associates, on behalf of their Client Mr. S. Rea, to undertake a traffic impact assessment for the proposed 270 Lot Residential Development to be located on the south-west periphery of Toolamba.

It is intended to review the existing and proposed road infrastructure, with respect to the additional traffic volumes and turning movements at external intersections, in support for the Residential Development.

This Traffic Impact Assessment Report has been prepared to ensure that any potential adverse effects from the proposed Development on road safety and operational efficiency are identified. The report will also address the following issues: -

- Review any previous traffic engineering assessments and any other relevant documents;
- Determination of traffic volumes generated by the proposed Residential Development;
- Impact of the proposed Residential Development on the existing infrastructure of Wren Street and Rutherford Road and the proposed internal roads;
- Determination of road widths to be adopted;
- Recommendations for any traffic management devices for the existing/new intersections;
- Pedestrian and cyclists infrastructure requirements;
- Impact of staged Development; and
- Recommendations for appropriate mitigating works.

2. Existing Conditions

2.1 Site Location

The site of the proposed residential neighbourhood is located on the south western side of Toolamba within a Farming Zone and is subject to Floodways overlays.

This site is currently used for grazing and cropping purposes.

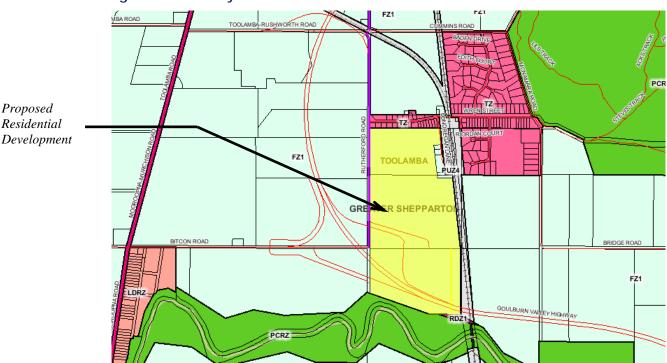


Figure 1 Locality Plan

Source: Department of Transport, Planning and Local Infrastructure; Planning Maps Online

The surrounding land uses are mainly Township and Farming, with public use (transport) zoning along the eastern side of the proposed development.

Through the southern portion of the proposed development is a public acquisition overlay identifying land which is proposed to be acquired for the Shepparton Bypass project.

2.2 Surrounding Street Network

The current entrance to the site is from Rutherford Road which is a sealed two-lane two-way traffic undivided rural road travelling in a north/south direction, with a regulatory speed limit of 100-km/h along the length of the Development. The seal width for Rutherford Road is in the order of 6.2m, with gravel shoulders approximately 1.0m wide, and has open drainage channels along both sides. Rutherford Road is currently classified as a rural access road.

Rutherford Road, north of the Wren Street intersection, is a sealed two-lane two-way traffic undivided rural road with a regulatory speed limit of 100-km/h and a seal width of 6.5m, with gravelled shoulders approximately 1.0m wide.

Close to the northern portion of the proposed development runs Wren Street, which is fronted by existing housing. Approximately 280m east of the Rutherford Road intersection, the proposed development connects with Wren Street via a part of the Rea land that resembles a vacant lot but is actually an undeveloped provision for access to the site. Wren Street is a sealed two-lane two-way traffic undivided rural street travelling in an east/west direction, with a regulatory speed limit of 50-km/h along the length of the Development. The seal width is in the order of 8.5m, with a 1.5m wide grass shoulder along its northern side and has type B2 kerbing along the southern side. Wren Street is classified as a Collector Level 1 road.

The Wren Street intersection with Rutherford Road is a T-intersection with central traffic island and a controlling Give-Way. There is an existing school bus stop approximately 40m north of the intersection, along the western side of Rutherford Road.

Rutherford Road is used predominately for the movement of cars and trucks from arterials or Rural Collectors for access to properties and farms, whereas Wren Street is mainly used for access to properties, farms or rural businesses.

2.3 Existing Traffic Flows

The peak traffic volumes utilising both Rutherford Road and Wren Street are detailed in Table 1.

Road Date		Traffic Volume – vpd	Hourly Pe AM	ak – vph PM	% Commercial Vehicles			
Source: Greater Shepparton	Source: Greater Shepparton City Council Traffic Counts (Appendix C)							
Rutherford Road – Nth of Intersection	24/10/2012	690	77	69	7.8			
Wren Street – East of Intersection	29/06/2006	797	55	88	3.3			
Bitcon Road	27/03/2009	242	19	29	6.6			
Bridge Road	19/12/2012	548	42	65	2.2			

 Table 1
 Two-way Weekday Traffic Count Summary

2.4 Crash Data

An examination of the VicRoads CrashStats database revealed, that for the last five years of available crash data, there have been no recorded casualty crashes along the lengths or within the vicinity of the proposed development, or at the intersection of Rutherford Road and Wren Street.

2.5 Impact of Shepparton Bypass

A western freeway bypass for Shepparton has been planned and approved. The course of the proposed bypass is to be located to the south and west of Toolamba, connecting with the Goulburn Valley Highway from Arcadia in the south to Congupna in the north.

The construction of the bypass will be undertaken in stages and is unlikely to occur for at least 10 years. The current proposal allows for the placement of both on and off ramps to be connected to Bitcon Road, which is also proposed to be extended through to Bridge Road in the east.

3. Proposed Development

The proposed development site is on the south-west periphery of Toolamba and will consist of 270 Residential Lots, which is to progress in 17 stages. Refer to Appendix A – Concept Plan for traffic assessment.

The Development will have access to and egress from both Rutherford Road and Wren Street. Ultimately, it is proposed that the development will be connected to the Bitcon Road – Bridge Road future extension.

However, for the purpose of this traffic impact assessment, this connection has been omitted due to the uncertainty of the freeway bypass construction timeframe.

It is considered that the volume of bypass interchange user traffic that may choose to access either the proposed development or the Toolamba Township via the road network that is to be analysed in this report, would have negligible impact on the analysis due to the traffic movements being very low in that regard.

Internally the development will have a central spine road – north/south alignment, through which the residential development is directly connected to both Wren Street to the north and ultimately to the Bitcon Road extension to the south.

To ensure that stages 15, 16 and 17 are not disconnected from the balance of the proposed development to the north and because of the uncertainty of the timing of the freeway bypass construction, the north-south central spine road is assumed to continue across the public acquisition overlay (where provision has been made for the future Bitcon Road extension). It has also been assumed that the future Bitcon Road extension will continue to maintain road access between stages 15, 16 and 17 and the balance of the proposed development to the north.

There will also be a connection to Rutherford Road from the centrally located east/west spine road. The Rutherford Road connection is approximately 370m south of the Wren Street intersection.

In considering the lot configuration, availability of sewer and services and Toolamba's unique small town appeal, the Developer contemplates that the development site may have a 'build out' horizon in the vicinity of 20 years.

This report acknowledges that VicRoads has an interest in the land which is subject to the Public Acquisition Overlay and that their future freeway design has not progressed beyond the preliminary phase.

Council has recently agreed to support a submission that proposes the Urban Growth Zone (UGZ) for the land. The rezoning to UGZ would run in conjunction with an application for approval of a "Precinct Structure Plan" (PSP).

The proposed staging of the residential development is as follows: -

Stage Number	Number of Lots	Frontage Facing	Main Entrance/Exit Point
1	15	Internal Street	Wren Street
2	16	Internal Street	Wren Street
3	19	Internal Street	Wren Street
4	22	Internal Street	Wren St / Rutherford Rd
5	10	Internal Street	Rutherford Road
6	16	External Street	Wren St / Rutherford Rd
7	22	Internal Street	Wren St / Rutherford Rd
8	16	Internal Street	Wren St / Rutherford Rd
9	13	Internal Street	Wren St / Rutherford Rd
10	11	Internal Street	Wren St / Rutherford Rd
11	17	Internal Street	Wren St / Rutherford Rd
12	19	Internal Street	Wren St / Rutherford Rd
13	15	Internal Street	Wren St / Rutherford Rd
14	15	Internal Street	Wren St / Rutherford Rd
15	15	Internal Street	Wren St / Rutherford Rd
16	15	Internal Street	Wren St / Rutherford Rd
17	14	Internal Street	Wren St / Rutherford Rd

Table 2 Proposed Subdivision Layout

4. Traffic Generation

Residential areas are the largest traffic generating land use category. Failure to estimate adequately the amount of traffic produced by a new subdivision can cause traffic problems on adjacent main roads and safety and environmental problems on internal roads.

Recent data from the Greater Shepparton City Council suggests that 10 vehicle trips per dwelling per day will provide characteristic traffic generation rates for a new subdivision – multi-car medium-high income suburb. For typical one car households in single family dwellings, the generation rate will be in the range of 6 to 8 vehicle trips per dwelling per day.

Typical relationship between peak hourly volumes and average daily traffic is 11% to 16% in rural situations.

Stages	Number of	Estimated Daily	Estimated Peak Hour
	Allotments	Traffic Volume	Traffic Volume
	(cumulative)	(two-way)	(two-way)
1, 2 & 3 – Wren St	50	500	57
5 – Rutherford Rd	10	100	11
Remaining 50/50	210	Wren & 1,050	Wren & 119
Split		Rutherford 1,050	Rutherford 119

Table 3 Traffic Generation Rates

Traffic generation for residential uses is typically tidal in nature, with the majority of vehicle movements during the AM peak hour occurring in the outbound direction, and traffic movements during the PM peak hour generally occurring in the inbound direction.

The traffic split can really only be determined by an origin/destination survey once the Development has been completed. But to ensure that any potential adverse impacts from the Development are identified early and any corrective measures designed, the following Traffic Flow Characteristic have been adopted based on the Approximations Related to Intersection Design¹, the RTA Guide to Traffic Generating Developments – October 2002 and the supplied existing traffic volume data from the Greater Shepparton City Council (refer to Appendix C): -

¹ Traffic Engineering and Practice – Chapter 8 Traffic Engineering Folklore, DW Bennett & KW Ogden, Monash University 1996

- 80% departing and 20% entering for the directional differences in morning peak flows;
- 30% departing and 70% entering for the directional differences in evening peak flows; and

An analysis will also be made on the movements based on the predicted year 20 values at a 0.5% p.a. growth rate for both Wren Street and Rutherford Road existing traffic volumes to ensure there will be no traffic related issues in the future.

Based on the supplied traffic volumes, it is assumed that of the traffic utilising Wren Street 50% will be turning west (left) and 50% will be turning east (right) at the intersection. As Wren Street provides easier access to the Toolamba Township, the assumed traffic split at the Rutherford entrance is that, 10% of the total volume will be turning south (left) to utilise Bitcon Road and 90% will be turning north (right) to utilise Rutherford Road and the Toolamba Rushworth Road to gain access to the arterial road network.

The anticipated maximum peak hourly traffic volumes at the intersections on the completion of the Development are: -

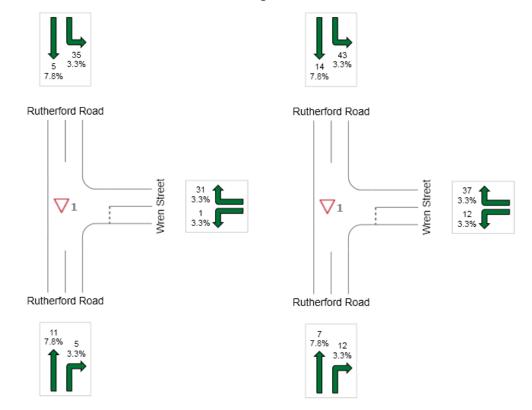
Location	Existing Tra	iffic Counts	Estimated at Completion (at Year 20 with 0.5% pa growth)		
	Vehicles	per Hour	Vehicles	per Hour	
	AM	PM	АМ	PM	
Wren Street					
Eastbound through	35	48	50	65	
Westbound through	28	42	32	49	
Left turn into Development			18	62	
Right turn into Development			18	62	
North/south entrance					
Left turn out of Development			71	27	
Right turn out of Development			71	27	
Rutherford Road - South of Wren					
Northbound through	14	17	16	19	
Southbound through	5	23	10	31	
Left turn into Development			23	82	
Right turn into Development			3	9	

Table 4 Site Generated Traffic Movements – Peak Hour

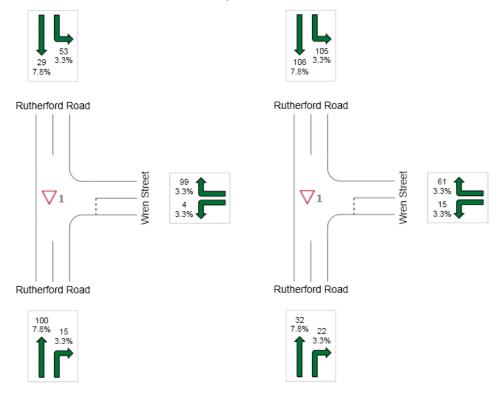
Location	Existing Tra	affic Counts	Estimated at Completion (at Year 20 with 0.5% pa growth)		
	Vehicles	per Hour	Vehicles	per Hour	
	AM	PM	AM	PM	
East/west entrance					
Left turn out of Development			10	4	
Right turn out of Development			94	35	
Wren/Rutherford					
Left turn out onto Rutherford			4	15	
Right turn out onto Rutherford			99	61	
Left turn into Wren			53	105	
Right turn into Wren			15	22	
Northbound through	11	7	100	32	
Southbound through	5	14	29	108	

Figure 2 Diagrams of Intersection Traffic Volumes

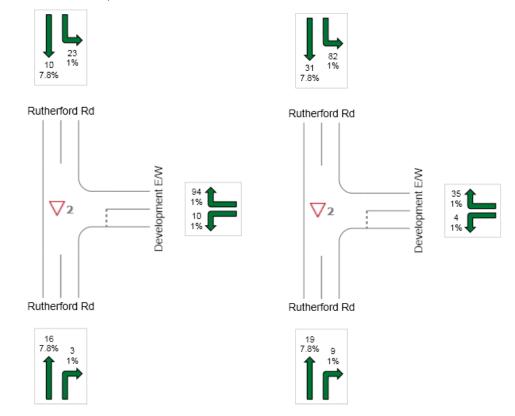
Wren St / Rutherford Rd Intersection Existing Conditions - AM & PM



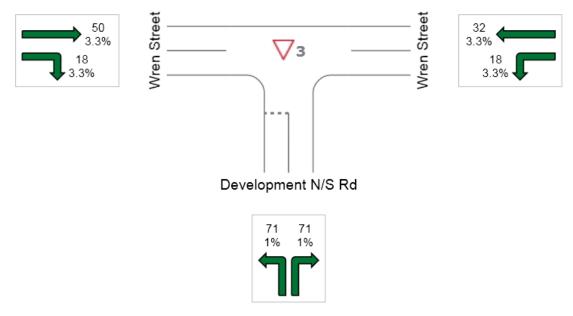
Wren St / Rutherford Rd Intersection Proposed Conditions - AM & PM

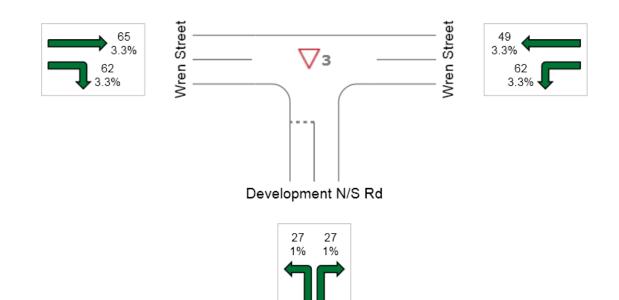


Rutherford Rd / Proposed East-West Rd Intersection – AM & PM



Wren St / Proposed North-South Rd Intersection - AM & PM





5. Intersection Analysis

The existing Rutherford Road and Wren Street intersection and the proposed entrances into the development are all T-intersections with through, left and right turning movements.

The operations of the intersections were analysed using SIDRA Intersection, during the AM and PM peak hours. This computer package, originally developed by the Australian Road Research Board, provides information about the capacity of an intersection in terms of a range of parameters, as described below:

- Degree of Saturation (DOS) is the ratio of the volume of traffic observed making a particular movement compared to the maximum capacity for that movement. Various values of degree of saturation and their rating are shown in Table 5.
- The 95th Percentile (95%ile) Queue represents the maximum queue length, in metres, that can be expected in 95% of observed queue lengths in the peak hour; and
- Average Delay is the delay time, in seconds, which can be expected over all vehicles making a particular movement in the peak hour.

Level of Service	Degree of Saturation	Traffic Signals and Roundabouts	Control Delay per Vehicle (sec/veh)	Give Way and Stop Signs	Control Delay per Vehicle (sec/veh)
A (excellent)	x ≤ 0.6	Good operation	d ≤ 10	Good operation	d ≤ 10
B (very good)	0.6 < x ≤ 0.7	Good with acceptable delays and spare capacity	10 < d ≤ 20	Acceptable delays and spare capacity	10 < d ≤ 15
C (good)	0.7 < x ≤ 0.8	Satisfactory	20 < d ≤ 35	Satisfactory but an accident study required	15 < d ≤ 25
D (acceptable)	0.8 < x ≤ 0.9	Operating near capacity	35 < d ≤ 55	Near capacity and accident study required	25 < d ≤ 35
E (poor)	0.9 < x ≤ 1.0	At capacity; at signals incidents will cause excessive delays and roundabouts require other control mode	55 < d ≤ 80	At capacity and requires other control mode	35 < d ≤ 50
F (very poor)	1.0 < x	Unsatisfactory and requires other control mode	80 < d	Unsatisfactory and requires other control mode	50 < d

Table 5Measures and Criteria

Source: RTA Guide to Traffic Generating Developments

For unsignalised intersections, a DOS of up to 0.80 is considered to be good operating conditions, with values above 0.90 considered to be poor operating conditions. Beyond a DOS of 1.00, queues and delays increase disproportionately.

Three scenarios were reviewed, the first was standard T-intersections with no auxiliary lanes, the second was all intersections were to be roundabouts and the third was to see the effects of one of the internal exit roads being blocked would have on the existing standard T-intersections layouts. A summary of the SIDRA results are shown below in Table 6, and a copy of the SIDRA output are attached at Appendix B.

Based on the output from the SIDRA analysis, the model results for the intersection during morning and evening peak times are: -

			lenning kesun					
			Existing Conditions			Post-development Conditions		
Approach		Movement	Degree of Saturation	95th%ile Queue (m)	Average Delay (s)	Degree of Saturation	95th%ile Queue (m)	Average Delay (s)
			EXISTING	T-INTERSECTIO	ON LAYOUTS			
Ruthe	erford / Wren							
	Rutherford Road	Through	0.009	0.2	0.1	0.067	0.1	0.0
	(South approach)	Right	0.009	0.2	7.6	0.067	0.1	7.7
eak	Rutherford Road	Through	0.023	0.0	0.0	0.047	0.0	0.0
AM Peak	(North approach)	Left	0.023	0.0	7.9	0.047	0.0	7.9
P	Wren Street	Right	0.027	0.6	4.7	0.099	0.3	5.3
	(East approach)	Left	0.027	0.6	4.6	0.099	0.3	4.7
	Rutherford Road	Through	0.012	0.1	0.1	0.035	1.0	0.5
	(South approach)	Right	0.012	0.1	7.6	0.035	1.0	8.2
PM Peak	Rutherford Road (North approach)	Through	0.033	0.0	0.0	0.122	0.0	0.0
MP		Left	0.033	0.0	7.9	0.122	0.0	7.9
	Wren Street	Right	0.040	0.1	4.8	0.073	1.8	5.5
	(East approach)	Left	0.040	0.1	4.6	0.073	1.8	5.0
Ruthe	erford / East-West	· · · · · · · · · · · · · · · · · · ·						
	Rutherford Road	Through				0.011	0.1	0.0
	(South approach)	Right				0.011	0.1	7.5
Peak	Rutherford Road	Through				0.019	0.0	0.0
AM Peak	(North approach)	Left				0.019	0.0	7.9
ł	Wren Street	Right				0.087	2.1	4.8
	(East approach)	Left				0.087	2.1	4.6
	Rutherford Road	Through				0.017	0.4	0.2
	(South approach)	Right				0.017	0.4	7.8
PM Peak	Rutherford Road	Through				0.065	0.0	0.0
MF	(North approach)	Left				0.065	0.0	7.9
	Wren Street	Right				0.034	0.8	5.0
	(East approach)	Left				0.034	0.8	4.7

Table 6 Modelling Results

			E	xisting Conditior	าร	Post-development Conditions			
	Approach	Movement	Degree of Saturation	95th%ile Queue (m)	Average Delay (s)	Degree of Saturation	95th%ile Queue (m)	Average Delay (s)	
Wrei	n / North-South	• •				•			
	Wren Street	Through				0.028	0.0	0.0	
	(East approach)	Left				0.028	0.0	4.6	
Peak	Wren Street (West approach)	Through				0.039	0.8	0.1	
AM Peak		Right				0.039	0.8	4.8	
4	North/South Road	Right				0.112	3.0	5.0	
	(South approach)	Left				0.112	3.0	4.7	
	Wren Street	Through				0.064	0.0	0.0	
	(East approach)	Left				0.064	0.0	4.6	
eak	Wren Street	Through				0.078	2.4	0.3	
PM Peak	(West approach)	Right				0.078	2.4	5.0	
<u> </u>	North/South Road	Right				0.045	1.1	5.4	
	(South approach)	Left				0.045	1.1	4.7	
		EXIST	ING T-INTERSE	CTION LAYOU	JTS WITH BLO	CKAGES			
Ruth	erford / Wren – Pro	posed North	/South Blocke	ed					
	Rutherford Road	Through				0.154	4.1	0.2	
	(South approach)	Right				0.154	4.1	7.8	
eak	Rutherford Road (North approach)	Through				0.047	0.0	0.0	
AM Peak		Left				0.047	0.0	7.9	
A	Wren Street (East approach)	Right				0.038	0.9	6.0	
		Left				0.038	0.9	4.7	
	Rutherford Road (South approach)	Through				0.069	2.2	0.6	
		Right				0.069	2.2	8.3	
eak	Rutherford Road	Through				0.125	0.0	0.0	
PM Peak	(North approach)	Left				0.125	0.0	7.9	
Δ.	Wren Street	Right				0.101	2.8	6.0	
	(East approach)	Left				0.101	2.8	5.2	
Ruth	erford / Wren – Pro	posed East/V	Vest Blocked	<u> </u>	<u>.</u>	<u> </u>			
	Rutherford Road	Through				0.019	0.6	0.2	
	(South approach)	Right				0.019	0.6	7.8	
eak	Rutherford Road (North approach)	Through				0.059	0.0	0.0	
AM Peak		Left				0.059	0.0	7.9	
A	Wren Street (East approach)	Right				0.184	4.9	5.0	
		Left				0.184	4.9	4.6	
	Rutherford Road (South approach)	Through				0.028	0.9	0.7	
		Right				0.028	0.9	8.3	
eak	Rutherford Road (North approach)	Through				0.139	0.0	0.0	
PM Peak		Left				0.139	0.0	7.9	
д_	Wren Street	Right				0.118	2.9	5.3	
	(East approach)	Left				0.118	2.9	4.7	

			E	xisting Condition	IS	Post-development Conditions			
	Approach	Movement	Degree of Saturation	95th%ile Queue (m)	Average Delay (s)	Degree of Saturation	95th%ile Queue (m)	Average Delay (s)	
Ruth	erford / East-West –	Proposed No	orth-South Blo	ocked			·		
	Rutherford Road	Through				0.011	0.1	0.0	
	(South approach)	Right				0.011	0.1	7.6	
Peak	Rutherford Road	Through				0.029	0.0	0.0	
AM Peak	(North approach)	Left				0.029	0.0	7.9	
	Wren Street	Right				0.209	5.6	4.8	
	(East approach)	Left				0.209	5.6	4.6	
	Rutherford Road	Through				0.017	0.4	0.3	
	(South approach)	Right				0.017	0.4	8.0	
Peak	Rutherford Road (North approach)	Through				0.101	0.0	0.0	
MP		Left				0.101	0.0	7.9	
	Wren Street (East approach)	Right				0.059	1.4	5.1	
		Left				0.059	1.4	4.7	
Wrer	Wren / North-South – Proposed East-West Blocked								
	Wren Street	Through				0.028	0.0	0.0	
	(East approach)	Left				0.028	0.0	4.6	
AM Peak	Wren Street	Through				0.054	1.5	0.1	
MF	(West approach)	Right				0.054	1.5	4.8	
4	North/South Road (South approach)	Right				0.182	5.5	5.2	
		Left				0.182	5.5	4.7	
	Wren Street (East approach)	Through				0.064	0.0	0.0	
		Left				0.064	0.0	4.6	
eak	Wren Street (West approach)	Through				0.133	4.7	0.4	
PM Peak		Right				0.133	4.7	5.0	
	North/South Road	Right				0.078	2.1	5.8	
	(South approach)	Left				0.078	2.1	4.7	

The outcomes of the SIDRA analysis in Table 6 can be summarised as follows: -

- This type of increase in traffic volume and change in operation of the intersection is considered to be indiscernible to the general motorist and is not expected to have any material impact on the operation of the surrounding road network. This is supported by the SIDRA Intersection analysis shown in Table 6, which identifies that 95th percentile queues and average delays at the Wren Street / Rutherford Road intersections are not expected to change due to the modest increase in traffic volumes that could be expected to be generated by the development shown in the concept plans.
- It is noted that both intersections currently operate under 'excellent' conditions during the AM and PM peak hours, and it is expected that they will continue to do so under the anticipated post-development traffic volumes; even when one entrance has become blocked.

6. Sight Distance

Intersection (*including driveways*) safety performance is dependent upon adequate horizontal and vertical sight distance for all entering traffic.

A feature of intersections is that sight lines are often required at large angles to the user's normal viewpoint. In a motor vehicle, the driver may have to look through the side windows. As well, the paths travelled are often significantly curved, which means that drivers find it more difficult to estimate stopping distances along the travel path.

The type and extent of sight distance available will significantly influence the design and location of an intersection. Both horizontal and vertical sight lines must be taken into account to check for disruption by natural objects, such as trees, and structures, such as fences, buildings and safety barriers.

The types of sight distance that must be provided in designing all intersections include: Approach Sight Distance (*ASD*), Safe Intersection Sight Distance (*SISD*) and Minimum Gap Sight Distance (*MGSD*).

Table 7 provides specific requirements for sight distance on level grades. The values in these tables refer to passenger cars only.

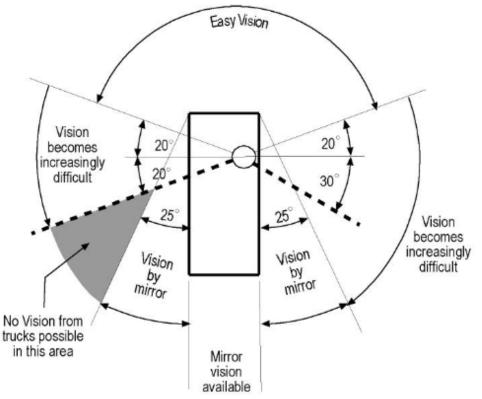


Figure 3 Sight Restrictions due to Vehicle Design

Source: Austroads Guide to Road Design Part 4A - Unsignalised & Signalised Intersections

6.1 Approach sight distance (ASD)

ASD is the minimum level of sight distance which must be available on the minor road approaches to all intersections. ASD is numerically equal to normal car stopping sight distance (*SSD*), which is defined as the distance travelled by a vehicle between the times when the driver receives a stimulus signifying a need to stop and the time the vehicle comes to rest.

The difference between ASD and SSD is the object height used in its calculation. ASD is measured from a driver's eye height (1.1m) to 0.0m, which ensures that a driver is able to see any line marking and kerbing at the intersection.

In circumstances where it is unreasonable or exceedingly difficult to achieve ASD, the design should provide, as an absolute minimum, SSD measured from a driver's eye height (1.1m) to an object height of 0.2m. This will ensure that signs and other road furniture at the intersection are clearly visible and provides a minimum standard to ensure that drivers are aware of the presence of an intersection.

6.2 Safe intersection sight distance (SISD)

SISD is the minimum standard that should be provided on the major road at any intersection. It provides sufficient distance for a driver of a vehicle on the major road to observe a vehicle on a minor road approach moving into a collision situation (e.g. in the worst case, stalling across the traffic lanes), and to decelerate to a stop before reaching the collision point. It is generally sufficient to enable cars to cross a major road safely from a side road.

SISD shall be provided at all intersections.

6.3 Minimum gap sight distance (MGSD)

MGSD is based on distances corresponding to the critical acceptance gap that drivers are prepared to accept when undertaking a crossing or turning manoeuvre at intersections.

MGSD is:

- measured from the point of conflict (between approaching and entering vehicles) back along the centre of the travel lane of the approaching vehicle
- measured from a point 1.1 m (driver's eye height) to a point 0.65 m (object height
 – typically a vehicle indicator light) above the travelled way.

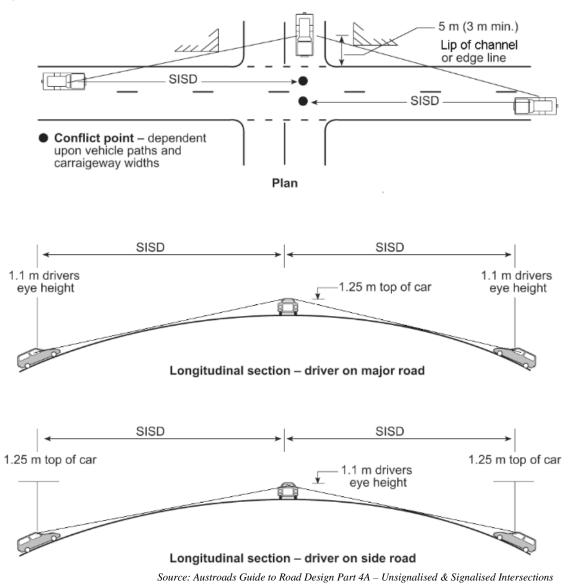
The MGSD required for the driver of an entering vehicle to see a vehicle in the conflicting streams in order to safely commence the desired manoeuvre is dependent upon the:

- > length of the gap being sought
- > observation angle to approaching traffic.

The critical acceptance gap time varies according to:

- the type of manoeuvre left-turn/right-turn/crossing
- > the width of carriageway increased time required for greater widths
- whether the major road has a one-way or two-way traffic flow increased time required to look both ways.





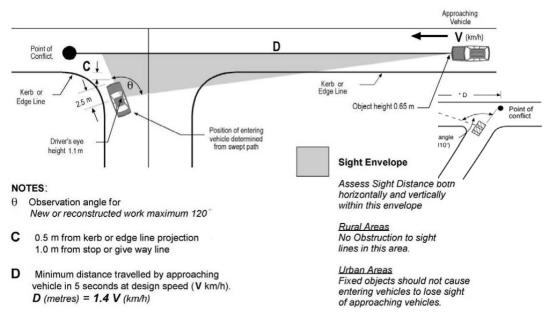


Figure 5 Sight Distance to a Through Vehicle – Left & Right Turn

Source: Austroads Guide to Road Design Part 4A – Unsignalised and Signalised Intersections

Table 7 Intersection Sight Distance for Level Grade

		h sight distance o 0.0m)	SISD - Safe intersection sight distance (1.1m to 1.25m)		
Design speed (major road) (km/h)	Absolute Desirable minimum 2.0 secs		Absolute minimum 1.5 secs	Desirable 2.0 secs	
	m	m	m	m	
40	34	40	67	73	
<mark>50</mark>	48	<mark>55</mark>	90	<mark>97</mark>	
60	64	73	114	123	
70	83	92	141	151	
80	103	114	170	181	
90	126	139	201	214	
<mark>100</mark>	151	<mark>165</mark>	234	<mark>248</mark>	

Source: Austroads Guide to Road Design Part 4A – Unsignalised and Signalised Intersections

Table 8 MGSD ('D' metres) for Various Speeds

Critical gap	85 th percentile speed of approaching vehicle (km/h)										
acceptance time (ta) (secs)	10	20	30	40	50	60	70	80	90	100	110
4	11	22	33	44	55	67	78	89	100	111	122
5	14	28	42	55	<mark>69</mark>	83	97	111	125	<mark>139</mark>	153
6	17	33	50	67	83	100	117	133	150	167	183
7	19	39	58	78	<mark>97</mark>	117	136	155	175	<mark>194</mark>	214
8	22	44	67	89	111	133	155	178	200	222	244
9	25	50	75	100	125	150	175	200	225	250	275
10	28	56	83	111	139	167	194	222	250	278	305

Source: Austroads Guide to Road Design Part 4A – Unsignalised and Signalised Intersections

6.4 Available Sight Distance

ASD requirements for the intersection and the entranceway are exceeded by the existing layouts.

The minimum requirements for SISD and MGSD are available at all approaches to the intersections along both Wren Street and the Rutherford Road.

The critical acceptance gap times for various manoeuvres into, from and across Wren Street and the Rutherford Road (see *table 9*), have been used within the SIDRA analysis to determine delays.

Movement	Critical Gap	Follow-up Headway
RHT – from major road	4.5 sec	2.5 sec
LHT – from minor road	5.0 sec	3.0 sec
RHT – from minor road	7.0 sec	4.0 sec

Table 9 Critical acceptance gaps and follow-up headways

7. Design Objectives

7.1 Road Hierarchy

In considering the classification, function and general composition of the road network, this report is guided by clause 12.3.2 of the Infrastructure Design Manual, version 4.3 dated 26 September 2014, which is prepared and maintained by the Local Government Infrastructure Design Association of which Greater Shepparton City Council is a member. The assigned road hierarchy for the proposed development is shown in Appendix A – Road Hierarchy Plan. The typical cross sections for the proposed roads are also shown in Appendix A – Typical Cross Sections-Road Reserves.

7.2 Pavement and Seal Widths

Table 10 below summarises the existing and proposed road characteristics: -

Road Name Classification (see note 1)		Maximum AADT Volume	Sealed Width (m)	Comments
Existing				
Wren Street	Collector Level 1			Has an existing sealed width of 6.8m
Rutherford Road	Rural Living Access			Has an existing sealed width of 6.2m south of Wren and 6.5m north of Wren
Proposed				
North/South spine	Collector Level 1	3,000	13.6	This is a modified cross section (see note 2)
East/West spine	Collector Level 1	3,000	13.6	This is a modified cross section (see note 2)
Other Internal	Access Street	1,000	7.5	The development does not propose to construct pavements less than 7.5 m width
Rutherford (East- West to Wren)	External Collector/Rural Living	3,000	9.9	This is a modified cross section (see note 3)

Table 10 Street and Rural Road Characteristics

Notes:-

- 1. The context of the road classification is what it would be if the road were to be constructed today.
- 2. This modified cross section allows for 2 no on road bicycle lanes each having 1.2m width and a shared path having a width of 2.5m on one side and footpath having a width of 1.5 on the other side.
- 3. This modified cross section is a hybrid that allows for road widening to achieve a 6.8 m width of seal on the east side fronting the development while maintaining the existing 3.1m width of seal on the west side

7.3 Design Speed Values

The existing regulatory speed restriction along Wren Street, which is to be continued within the Development, is 50-km/h.

It is recommended that along the internal street, that slow points be installed between 100m to 140m apart to ensure that the required 30 to 50-km/h speed restrictions are maintained along their lengths.

The types of slow point to be installed to meet the objective of reduced mid-block traffic speeds are Parallel, Angled or Offset – all of which have the potential for landscaping.

Rutherford Road has a current regulatory speed limit of 100-km/h, along both approaches to Wren Street, which needs to be reviewed as the development progresses along Rutherford Road and/or the construction of the Shepparton Bypass.

Based on VLimits, the speed limit along Rutherford Road needs to be reduced to 50-km/h once Stage 5 has been completed.

7.4 Pedestrians and Cyclists

7.4.1 Pedestrians

Pedestrians form the largest single road-user group. Nearly all short trips could be undertaken on foot and even longer trips, whether the main mode of transport is by private car, public transport or cycling - require the road user to be a pedestrian at some stage of the journey. Walking is a key element in the way Australians travel to work, school and local facilities.

Planning and designing good pedestrian infrastructure with well-connected and amenable facilities will benefit the whole community.

Pedestrian networks should be planned in combination with land uses to provide residential access to mixed use centres and be designed with passive surveillance and good lighting to provide an attractive and safe walking environment.

Some of the design requirements for designing pedestrian infrastructure are: -

- > Minimum path widths for different pedestrians
 - Pedestrians in a wheelchair 1.2m
 - Pedestrian in wheelchair passing pram 1.5m
 - Two pedestrians in wheelchairs passing 1.8m
- > Minimum pedestrian through route width
 - 1.2m over short distance (allows 1 wheelchair)
 - 1.8m desirable to allow 2 wheelchairs to pass (1.5m minimum), 2m near schools and small shops
 - At least 2.4m in commercial or shopping environments
 - 3m 4m in busy C.B.D pedestrian area
- Installation of Tactile Ground Surface Indicator's
 - Warning TGSI positioned 0.3m from edge of hazard, perpendicular to the direction of travel and across the entire ramp width preferred depth of 0.8m (minimum 0.6m)
 - Directional TGSI used where a person has to deviate from their path of travel to access a facility, at a minimum width of 0.8m. Also used to guide pedestrian through complicated area, at a minimum width of 0.3m.
- Non-Signalised Intersections
 - Design details such as kerb radii and provision of refuges or kerb extensions can greatly influence pedestrian safety at unsignalised intersections.
 Recommended kerb radii are 6m for local access streets and 9m for intersections with neighbourhood connectors
- Roundabouts
 - Roundabouts should be designed with adequate entry curvature or deflection to reduce the speed of approaching vehicles. Recommended to locate kerb ramps and median cut throughs at least 6m from the vehicle holding line (1 - 2 car lengths)

Currently within Toolamba the footpath surface and access vary, including designated concrete footpaths at the General Store and Hotel, but mostly the footpaths are gravel, dirt or sealed road shoulders.

7.4.2 Proposed Pedestrian Network Plan

A proposed Pedestrian Network Plan for this Development has been developed detailing the use of shared paths and noting that all internal streets to have a pedestrian path on both sides (refer to Appendix A).

7.4.3 Cyclists

The provision of a footpath, shared path and/or a bicycle lane from the development is required to provide a link to the recreational areas, schools and to the shopping precinct.

The requirements set out below are based on the Greater Shepparton City Council's Infrastructure Design Manual and discussions with the Councils Development Branch.

- A footpath is required on both sides of streets classified as a Residential Court Bowl, to facilitate pedestrian and bicycle movements. No separate provisions for cyclists are required.
- Along Access Streets, footpaths are required on both sides of the street to facilitate pedestrian and bicycle movements. No separate provisions for cyclists are required.
- For the Collector Streets, footpaths will be required along both sides of the street with on road bike lanes – or the footpaths are widened to be classified as shared paths. As this shared path will be utilised for both commuting and local access purposes, the minimum width is to be 2.5m.
- With respect to car parks and pedestrian paths along Rutherford Road where there are residential lots on one side only, car parking and pedestrian paths would only be required on one side of the road. Consideration needs to be given to linking the pedestrian path to the shared path network in the land where there are lots on one side only.

The City of Greater Shepparton in 2009 produced a cycling guide and in December 2013 the revised Bicycle Strategy was finalised, which provides a framework for the provision of a network of bicycle paths throughout the Greater Shepparton area.

The Guide provided a variety of routes to ride, including the Toolamba Circuit and the Tatura Toolamba Circuit.

One of the recommendations of the Bicycle Strategy (based on public consultation meeting held within the region), is to provide direct, preferably off-road cycling paths between key towns and destinations within cycling distance. Suggested examples included: -

- Murchison Toolamba Shepparton
- > Tatura Toolamba
- > Toolamba Old Toolamba

The needs of bicycle users and their requirements for an efficient and usable bicycle network require coherence, directness, safety, attractiveness and comfort.

Bicycle network infrastructure should form a coherent unit by linking popular destinations with local residential streets via regional and local routes. Intersections should seek to provide a clear path for bicycle riders as well as for other modes.

A major consideration in the provision of bicycle operating space on rural roads is the speed of other traffic. Where comfortable and safe sharing of a road is not achievable due to high speeds, some form of separation is needed such as sealed shoulders or off-road paths. When creating links in a rural bicycle transport system, which will make riding an attractive and desirable transport option, it is sometimes more economical to build off-road connecting paths (designed to carry only bicycles and pedestrian traffic) rather than sealed shoulders which have to be constructed to bear the loads of heavy vehicles. This has to be balanced with other factors associated with separate off-road paths: remoteness of facility; connectivity; maintenance etc.

In regional towns where street corridors are wide, sharing of road space is an easy option but careful attention must be paid to intersections. The main aim of the bicycle facilities is to guide the user along a clear and unambiguous path through all intersections along a route.

If the bicycle facility is part of a bicycle network route, separation is advisable in order to provide an adequate level of service and safety. The degree of separation required is largely dependant upon the prevailing speed and traffic volume of the road – see Figure 6. The amount of space available and the way existing space is distributed within the road reserve are other important issues to be considered. Where the facility is to be located in low volume and low speed a mixed traffic road profile can be safely considered. Where a road is to be fitted with bicycle facilities, which are not part of the bicycle network, shared facilities are more commonly used.

The road shoulder is suitable for regional and local bicycle network routes in moderate to low speed environments – see Figure 6.

There are currently no dedicated bicycle facilities provided in the township of Toolamba. This is in part due to its current size and limited number of trip generators.

7.4.4 Separating Cyclists from Pedestrians.

The most effective way to increase the capacity of off-road facilities for cyclists and pedestrians is to separate the user types by providing a separate footpath and a separate bicycle path.

The benefits of separation are increased capacity, safety and Level of Service.

Separating cyclists from pedestrians recognises the speed differential between cyclists and pedestrians and reduces the number of delayed passing that cyclists experience along a path. Separation also allows cyclists to maintain higher speeds, reduces the potential for conflict between cyclists and pedestrians and improves the level of service for pedestrians, especially elderly or disabled pedestrians.

7.4.5 Proposed Bicycle Network Plan

A proposed Bicycle Network Plan for this Development has been developed detailing the use of on-road bicycle lanes and shared paths (refer to Appendix A).

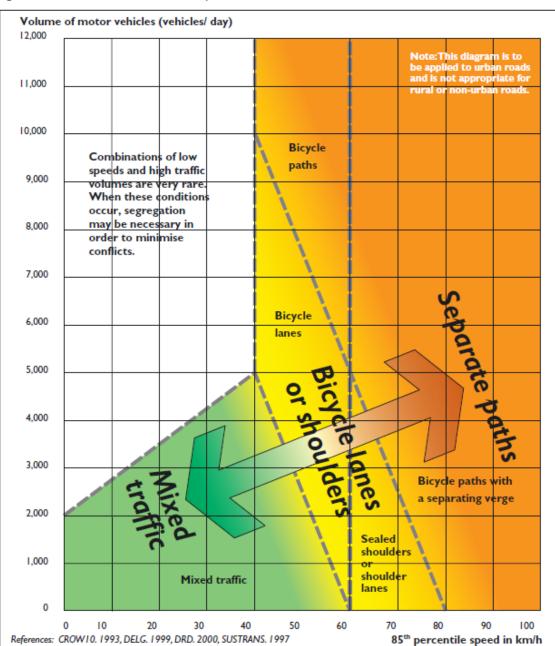


Figure 6 Minimum levels of separation

7.5 Street Lighting

Performance and design requirements of lighting are based on an assessment of degree of activity, risk of crime and the required aesthetic appeal.

The objective of street lighting is to provide: -

- > increased levels of lighting at focal points and hazardous locations.
- lighting in locations where pedestrians are required to make decisions regarding their safety.

Illumination level requirements are detailed in AS/NZS1158.1.1 – 2005 (vehicular traffic lighting), AS/NZS1158.3.1 – 2005 (lighting for pedestrian areas) and AS/NZS1158.4 – 2009 (supplementary lighting for pedestrian crossings).

Any lighting provided must be designed such that if one source fails, a second will continue to provide at least some light and the minimum design requirements are: -

- Lighting along Roadways
 - Local roads require minimum pedestrian lighting level of P3/P4/P5
 - Collector roads require minimum pedestrian lighting level of P3/P4
 - Arterial roads are to be designed to a minimum vehicular lighting level of V3
- > Lighting level for Pedestrian and Cyclists Pathways
 - Pathways are to be lit to a minimum horizontal and vertical illuminance of 5 lux, with a minimum of 20 lux at sites with high pedestrian volumes or conflict
- > Lighting Pole Design for Pedestrian and Cyclists Pathways
 - Poles should be setback from path by 0.8m 1m (0.5m absolute minimum for cyclist paths)
 - Pedestrian lights to be mounted at a height of 7m, with the outreach arm length between 0 to 1.5m
- Lighting level for Pedestrian Crossings
 - Minimum horizontal illuminance on a marked pedestrian crossing is 30 lux, except for sites with low pedestrian and traffic volumes where it may be reduced to 20 lux
- > Light pole placement along footpaths
 - Light poles (and other street furniture) should be placed outside the pedestrian through-route zone (desirable minimum width of 1.5m, absolute minimum width of 1.2m)

Within the stages of the development, the following lighting categories will be required: -

Table 11Lighting Category

Street Characteristics	Lighting Category
Residential Court Bowl	P5
Access Streets	P4
Connector Street – Level 1	P3

7.6 Intersection Type

The form of rural intersection control and traffic flows are the key crash risk factors associated with designing a rural intersection.

7.6.1 Priority-Controlled Intersections

Improvement of the safety performance of rural road priority-controlled intersections should be based on the following general principles: -

- minimise the number of high-exposure, high-speed conflict points,
- > establish clear priority for movements through the intersection,
- separate conflict points in space (e.g. auxiliary lanes) and time (traffic signals),
- control the angle of conflict; crossing streams of traffic should intersect at a rightangle or close to it, while merging streams should intersect at small angles to ensure low relative speed between the vehicles,
- control approach speeds using alignment, lane width, traffic control, speed limits, and ITS (e.g. vehicle activated signs),
- define and minimise conflict areas,
- provide adequate sight distances,
- minimise roadside hazards,
- provide for all vehicular and non-vehicular traffic likely to use the intersection, including where necessary, special provisions for heavy vehicles, public transport vehicles, pedestrians and other vulnerable road users.

A safe infrastructure solution will seek to: -

- 1. minimise opportunities for impacting other road users by separating conflicting movements (e.g. exclusion, separation),
- reduce impact speeds to survivable levels (e.g. < 50 km/h for right-angle impacts) if impacts are inevitable,

3. minimise impact force transfer to road users in other ways, e.g. by reducing vehicle angles, changing vehicle impact areas (e.g. from side to rear), extending crash duration, or by redirecting vehicles.

7.6.2 Roundabouts

A rural roundabout is inherently safer than a comparable priority-controlled or signalised intersection.

A key contributor to the safer operation of roundabouts is the relatively low intersection negotiation speed and the inherent expectation to give way. Speed of less than 50 km/h should be achieved prior to the vehicle entering the circulating lanes of the roundabout. Thus, approach speeds on rural roads will typically need to be reduced. Methods to achieve this involve using a series of curves on the approach, as outlined in the Guide to Road Design - Part 3 (Austroads 2010) and in Part 4B (Austroads 2011). This can be difficult to achieve in practice.

One of the solutions to approach speed dissipation problems is to avoid multi-lane roundabouts where possible. For the majority of rural roundabouts, delay and queuing are minor considerations, and approach capacity may not be needed – design provisions can be made for future expansion.

8. Concluding Remarks & Recommendations

8.1 Analysis

- This Traffic Impact Assessment has investigated the potential impacts of the traffic from the proposed 270 Lot Residential Development on the existing traffic operations of Wren Street and the surrounding Roads.
- Based on the projected number of total daily trips estimated for the proposed Residential Development and the predicted trip distribution, the impact on Wren Street and other surrounding roads will be minimal and any marginal traffic increase will be well within the capacity and function of these roads.
- The results in Table 6 further indicate that the existing and proposed intersection forms are readily able to accommodate the post development peak hour traffic volumes, with
 - low degrees of saturation, queue lengths and delays along both Wren Street and Rutherford Road, and
 - low degrees of saturation and queue lengths and delays at the connecting intersections to the development.
- The moderate traffic volumes generated from the proposed Development have been modelled using the SIDRA software. The results demonstrate that adequate capacity is available at the existing and proposed T-intersections. However, it may be appropriate that their operation be reviewed at some future stage, particularly at or around the construction of the bypass or after say 50% (Stage 8) build out of the development. If improved safety of these intersections is required, either auxiliary turn lanes (short) or roundabouts can be installed at each of the intersections.

The actual treatment to be adopted will be dependent upon: -

- Available road reserve width
- Value placed on the reduction of on-street car parking opportunities
- The use of shared or separate paths for pedestrians and cyclists
- Ensuring that vehicle speeds are to be less than 50-km/h along the development
- Relocation and/or modification of existing assets (e.g. existing School Bus Stop, table drains, etc.)
- The proposed new intersections (Wren / North-South and Rutherford / East-West) have minimal disruption to weekday through traffic on the existing road and they also have uninterrupted sightlines (although it is anticipated that a number of young trees are to be removed/trimmed at the proposed Wren / North-South intersection) ensuring safety is maximised.

- The traffic volume and parking demands likely to be generated as a result of this Residential Development is adequately provided for by the internal road network and private parking provisions.
- Street lighting will be required at the intersections to the Development and within the internal roads.
- To ensure connectivity with Council's Bicycle Strategy and Walking Guide, the Developer is to provide footpaths and on-road bike lanes – or footpaths that are widened to be classified as shared paths. As this shared path will be utilised for both commuting and local access purposes, the minimum width of 2.5m is recommended.
- The provision of slow points (shifting of vehicle paths laterally) between 100m to 140m apart are required along the main north/south and east/west streets to ensure that the required 30 to 50-km/h speed restrictions are maintained along their lengths.
- Based on the analysis undertaken the recommended trigger points for various works are as follows: -
 - Construction of the Wren Street / North-South intersection at Stage 1.
 - Linemarking of pedestrian/cyclist facilities along Wren Street (Rutherford Road to Londregan Lane) at Stage 5.
 - Construction of the Rutherford Road / East-West intersection at Stage 4 including the reduction of the existing 100-km/h speed zone to 50-km/h, commencing at the southern end of the development, along Rutherford Road to Wren Street. This point is also the anticipated connection point to the future on-ramp to the Shepparton Bypass to Melbourne.
 - A review of the Wren Street / Rutherford Road intersection operation at Stage 8, including the reduction of the existing 100-km/h speed zone to 80-km/h, commencing from Wren Street to Toolamba-Rushworth / Rutherford Road intersection.
 - Construction of pedestrian/cyclist facilities along Rutherford Road (Rutherford Road / East-West) to Wren Street at the completion of Stage 5.
- Accordingly, it is concluded the traffic related issues should not form an impediment to the approval of this Residential Development.

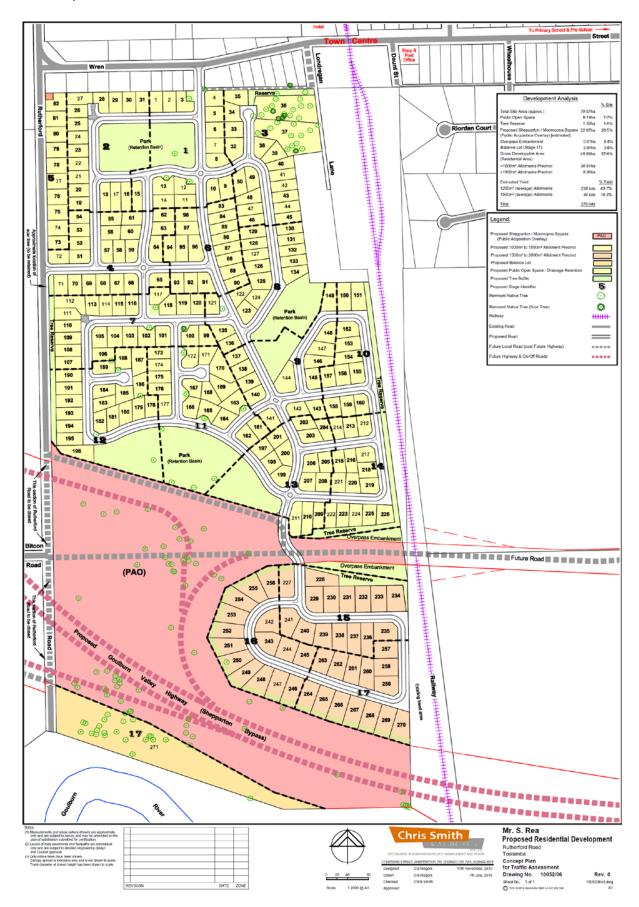
8.2 Pre Shepparton Bypass

- > Stages 15, 16 and 17 will be able to be connected to the main north/south road.
- In conjunction with Council, look into the feasibility to provide pedestrian/cyclist access to the Goulburn River via either Rutherford Road or the rail reserve, with the provision of end-of-trip facilities.

8.3 Post Shepparton Bypass

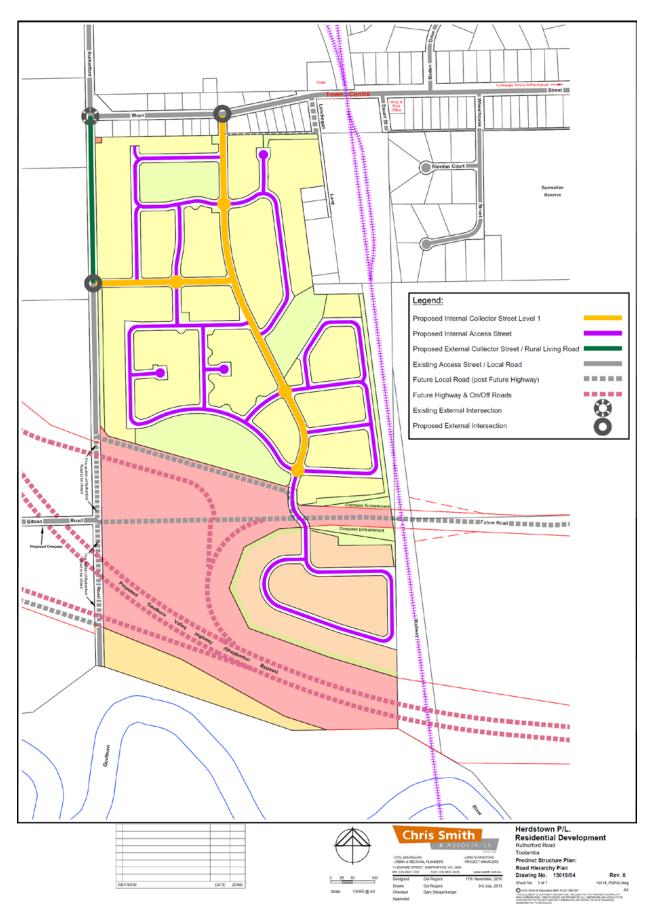
- The Bitcon Road extension is to continue to facilitate connectivity of Stages 15, 16 and 17 to the balance of the Development via the north-south spine road.
- Any existing or proposed pedestrian/cyclist access to the Goulburn River along Rutherford Road is to follow the altered road alignment to the Bitcon Road extension and connect to the rail reserve and pass under two road grade separations for continuation to the Goulburn River.
- Most of the traffic generation utilising the Shepparton Bypass within this region will be from the west of Toolamba, which has a denser regional demographic than the north-eastern side, hence utilising Bitcon Road. The additional traffic utilising Rutherford Road or the North-South internal road will mainly come from the township itself, which have the spare capacity to cater for this increase without detriment to the road user.

APPENDIX A Plans

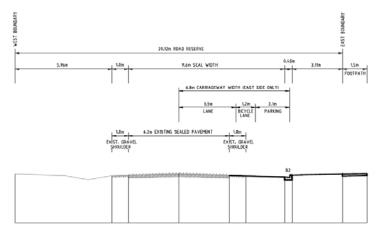


Concept Plan for Traffic Assessment

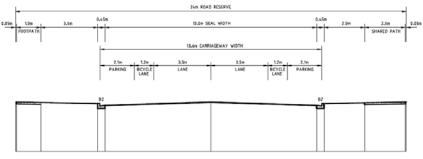
Road Hierarchy Plan



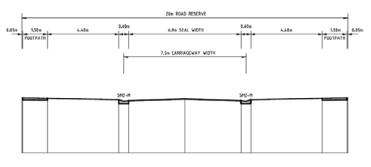
Typical Cross Sections - Road Reserve



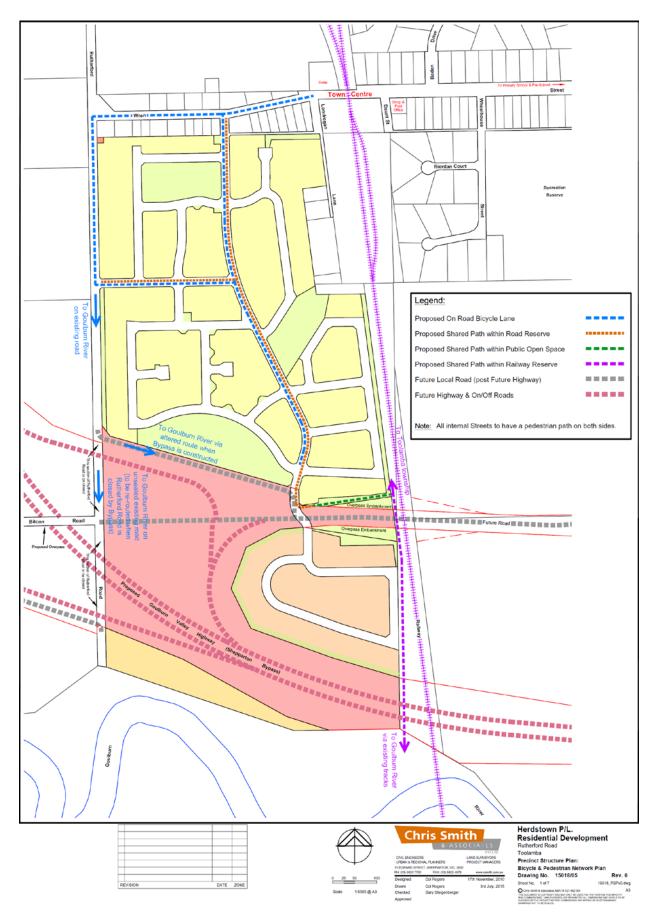
TYPICAL CROSS SECTION - EXTERNAL COLLECTOR / RURAL LIVING (RUTHERFORD ROAD - LOTS FRONTING)



TYPICAL CROSS SECTION - INTERNAL COLLECTOR LEVEL 1

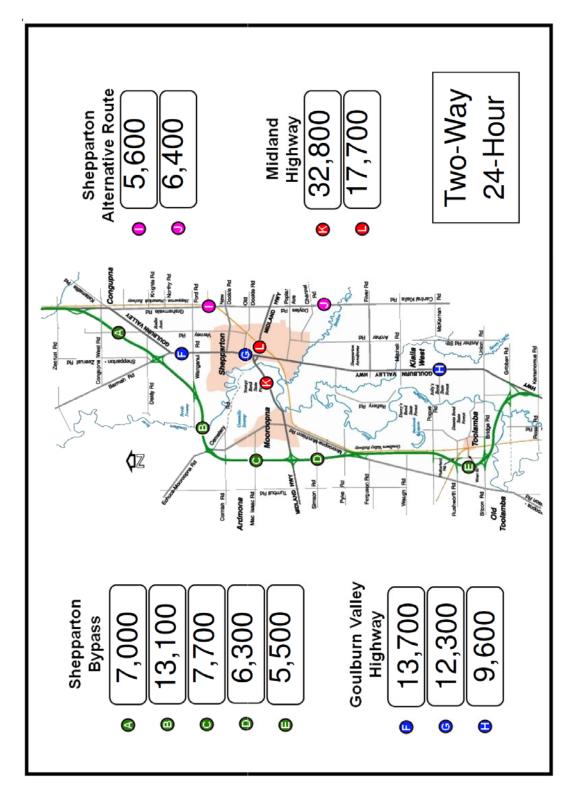


TYPICAL CROSS SECTION - INTERNAL ACCESS STREET



Proposed Pedestrian & Bicycle Network Plan

Traffic Volumes – All Traffic (2041)



APPENDIX B Intersection Analysis

Movement Summaries

$\overline{\nabla}$ Site: Rutherford Wren Existing AM Peak

Existing Rutherford Road / Wren Street Intersection Giveway / Yield (Two-Way)

Mover	Movement Performance - Vehicles Mov OD Demand Flows Deg. Average Level of 95% Back of Queue Prop. Effective Average													
Mov ID	OD Mov	Demand I Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h			
South:	Rutherford	Road												
2	T1	12	7.8	0.009	0.1	LOS A	0.0	0.2	0.08	0.21	92.0			
3	R2	5	3.3	0.009	7.6	LOS A	0.0	0.2	0.08	0.21	61.8			
Approa	ich	17	6.4	0.009	2.4	NA	0.0	0.2	0.08	0.21	81.9			
East: V	Vren Street	t												
4	L2	1	3.3	0.027	4.6	LOS A	0.1	0.6	0.09	0.54	53.2			
6	R2	33	3.3	0.027	4.7	LOS A	0.1	0.6	0.09	0.54	57.4			
Approa	ich	34	3.3	0.027	4.7	LOS A	0.1	0.6	0.09	0.54	57.3			
North:	Rutherford	Road												
7	L2	37	3.3	0.023	7.9	LOS A	0.0	0.0	0.00	0.58	51.9			
8	T1	5	7.8	0.023	0.0	LOS A	0.0	0.0	0.00	0.58	82.0			
Approa	ich	42	3.9	0.023	6.9	NA	0.0	0.0	0.00	0.58	54.6			
All Veh	icles	93	4.1	0.027	5.3	NA	0.1	0.6	0.05	0.50	59.2			

MOVEMENT SUMMARY

∇ Site: Rutherford Wren Existing PM Peak

Movement Performance - Vehicles Mov OD Demand Flows Deg. Average Level of 95% Back of Queue Prop. Effective Average													
Mov ID	OD Mov	Demand I Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/t		
South:	Rutherford		70	110	300		Von			perven	KITET		
2	T1	7	7.8	0.012	0.1	LOS A	0.1	0.4	0.14	0.40	85.5		
3	R2	13	3.3	0.012	7.6	LOS A	0.1	0.4	0.14	0.40	57.9		
Approa	ich	20	5.0	0.012	4.9	NA	0.1	0.4	0.14	0.40	67.4		
East: V	Vren Street	t											
4	L2	13	3.3	0.040	4.6	LOS A	0.1	1.0	0.08	0.53	53.2		
6	R2	39	3.3	0.040	4.8	LOS A	0.1	1.0	0.08	0.53	57.4		
Approa	ich	52	3.3	0.040	4.8	LOS A	0.1	1.0	0.08	0.53	56.5		
North:	Rutherford	Road											
7	L2	45	3.3	0.033	7.9	LOS A	0.0	0.0	0.00	0.51	52.7		
8	T1	15	7.8	0.033	0.0	LOS A	0.0	0.0	0.00	0.51	84.0		
Approa	ich	60	4.4	0.033	6.0	NA	0.0	0.0	0.00	0.51	58.5		
All Veh	icles	132	4.1	0.040	5.3	NA	0.1	1.0	0.05	0.50	58.8		

✓ Site: Rutherford Wren + Development AM Peak

Existing Rutherford Road / Wren Street Intersection Giveway / Yield (Two-Way)

Move	Movement Performance - Vehicles Mov OD Demand Flows Deg. Average Level of 95% Back of Queue Prop. Effective Average													
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h			
South:	Rutherford	Road												
2	T1	105	7.8	0.067	0.0	LOS A	0.1	0.7	0.06	0.09	96.0			
3	R2	16	3.3	0.067	7.7	LOS A	0.1	0.7	0.06	0.09	64.3			
Approa	ach	121	7.2	0.067	1.1	NA	0.1	0.7	0.06	0.09	91.5			
East: V	Vren Street													
4	L2	4	3.3	0.099	4.7	LOS A	0.3	2.4	0.23	0.57	52.6			
6	R2	104	3.3	0.099	5.3	LOS A	0.3	2.4	0.23	0.57	56.8			
Approa	ach	108	3.3	0.099	5.3	LOS A	0.3	2.4	0.23	0.57	56.7			
North:	Rutherford	Road												
7	L2	56	3.3	0.047	7.9	LOS A	0.0	0.0	0.00	0.44	53.5			
8	T1	31	7.8	0.047	0.0	LOS A	0.0	0.0	0.00	0.44	85.9			
Approa	ach	86	4.9	0.047	5.1	NA	0.0	0.0	0.00	0.44	62.4			
All Veh	icles	316	5.2	0.099	3.6	NA	0.3	2.4	0.10	0.35	68.7			

MOVEMENT SUMMARY

▽ Site: Rutherford Wren + Development PM Peak

Mover	nent Perf	ormance - V	ehicles								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South:	Rutherford		70	v/G	366		VGII			регусп	KIIVII
2	T1	34	7.8	0.035	0.5	LOS A	0.1	1.0	0.26	0.27	88.0
3	R2	23	3.3	0.035	8.2	LOS A	0.1	1.0	0.26	0.27	59.5
Approa	ich	57	6.0	0.035	3.6	NA	0.1	1.0	0.26	0.27	75.7
East: V	Vren Street	t									
4	L2	16	3.3	0.073	5.0	LOS A	0.2	1.8	0.26	0.57	52.5
6	R2	64	3.3	0.073	5.5	LOS A	0.2	1.8	0.26	0.57	56.6
Approa	ich	80	3.3	0.073	5.4	LOS A	0.2	1.8	0.26	0.57	55.9
North:	Rutherford	Road									
7	L2	111	3.3	0.122	7.9	LOS A	0.0	0.0	0.00	0.33	54.7
8	T1	114	7.8	0.122	0.0	LOS A	0.0	0.0	0.00	0.33	88.8
Approa	ich	224	5.6	0.122	3.9	NA	0.0	0.0	0.00	0.33	68.7
All Veh	icles	361	5.1	0.122	4.2	NA	0.2	1.8	0.10	0.38	66.5

▽ Site: Rutherford Wren + Development AM Peak - N/S Blocked

Existing Rutherford Road / Wren Street Intersection Giveway / Yield (Two-Way)

Move	ment Perf	ormance - V	ehicles								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South:	Rutherford	Road									
2	T1	180	7.8	0.154	0.2	LOS A	0.6	4.1	0.14	0.22	90.7
3	R2	91	3.3	0.154	7.8	LOS A	0.6	4.1	0.14	0.22	61.1
Approa	ich	271	6.3	0.154	2.7	NA	0.6	4.1	0.14	0.22	80.1
East: V	Vren Street	t									
4	L2	4	3.3	0.038	4.7	LOS A	0.1	0.9	0.25	0.58	52.1
6	R2	33	3.3	0.038	6.0	LOS A	0.1	0.9	0.25	0.58	56.3
Approa	ich	37	3.3	0.038	5.8	LOS A	0.1	0.9	0.25	0.58	55.9
North:	Rutherford	Road									
7	L2	37	3.3	0.047	7.9	LOS A	0.0	0.0	0.00	0.29	55.3
8	T1	49	7.8	0.047	0.0	LOS A	0.0	0.0	0.00	0.29	90.1
Approa	ich	86	5.9	0.047	3.4	NA	0.0	0.0	0.00	0.29	71.9
All Veh	icles	394	5.9	0.154	3.1	NA	0.6	4.1	0.12	0.27	75.2

MOVEMENT SUMMARY

▽ Site: Rutherford Wren + Development PM Peak - N/S Blocked

Move	nent Perf	ormance - V	ehicles								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South:	Rutherford	Road									
2	T1	59	7.8	0.069	0.6	LOS A	0.3	2.2	0.29	0.31	86.7
3	R2	52	3.3	0.069	8.3	LOS A	0.3	2.2	0.29	0.31	58.6
Approa	ich	111	5.7	0.069	4.2	NA	0.3	2.2	0.29	0.31	72.9
East: V	Vren Street										
4	L2	81	3.3	0.101	5.2	LOS A	0.4	2.8	0.30	0.56	52.2
6	R2	39	3.3	0.101	6.0	LOS A	0.4	2.8	0.30	0.56	56.4
Approa	ich	120	3.3	0.101	5.5	LOS A	0.4	2.8	0.30	0.56	53.7
North:	Rutherford	Road									
7	L2	45	3.3	0.125	7.9	LOS A	0.0	0.0	0.00	0.13	57.3
8	T1	184	7.8	0.125	0.0	LOS A	0.0	0.0	0.00	0.13	95.1
Approa	ich	229	6.9	0.125	1.6	NA	0.0	0.0	0.00	0.13	84.9
All Veh	icles	460	5.7	0.125	3.2	NA	0.4	2.8	0.15	0.29	72.4

▽ Site: Rutherford Wren + Development AM Peak - E/W Blocked

Existing Rutherford Road / Wren Street Intersection Giveway / Yield (Two-Way)

Mover	nent Perf	ormance - V	ehicles								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South:	Rutherford	Road									
2	T1	17	7.8	0.019	0.2	LOS A	0.1	0.6	0.18	0.31	87.6
3	R2	16	3.3	0.019	7.8	LOS A	0.1	0.6	0.18	0.31	59.2
Approa	ich	33	5.6	0.019	3.9	NA	0.1	0.6	0.18	0.31	73.1
East: V	Vren Street										
4	L2	11	3.3	0.184	4.6	LOS A	0.7	4.9	0.15	0.55	53.0
6	R2	207	3.3	0.184	5.0	LOS A	0.7	4.9	0.15	0.55	57.2
Approa	ich	218	3.3	0.184	5.0	LOS A	0.7	4.9	0.15	0.55	57.0
North:	Rutherford	Road									
7	L2	96	3.3	0.059	7.9	LOS A	0.0	0.0	0.00	0.60	51.7
8	T1	11	7.8	0.059	0.0	LOS A	0.0	0.0	0.00	0.60	81.6
Approa	ich	106	3.7	0.059	7.1	NA	0.0	0.0	0.00	0.60	53.8
All Veh	icles	357	3.6	0.184	5.5	NA	0.7	4.9	0.11	0.54	57.1

MOVEMENT SUMMARY

▽ Site: Rutherford Wren + Development PM Peak - E/W Blocked

Move	Movement Performance - Vehicles Mov OD Demand Flows Deg. Average Level of 95% Back of Queue Prop. Effective Average													
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/t			
South:	Rutherford		70	V/G	366		VGII			регусп	KIIVI			
2	T1	20	7.8	0.028	0.7	LOS A	0.1	0.9	0.32	0.35	85.3			
3	R2	23	3.3	0.028	8.3	LOS A	0.1	0.9	0.32	0.35	57.8			
Approa	ach	43	5.4	0.028	4.8	NA	0.1	0.9	0.32	0.35	69.9			
East: V	Vren Street	t												
4	L2	4	3.3	0.118	4.7	LOS A	0.4	2.9	0.24	0.57	52.6			
6	R2	123	3.3	0.118	5.3	LOS A	0.4	2.9	0.24	0.57	56.8			
Approa	ach	127	3.3	0.118	5.3	LOS A	0.4	2.9	0.24	0.57	56.6			
North:	Rutherford	Road												
7	L2	220	3.3	0.139	7.9	LOS A	0.0	0.0	0.00	0.58	51.9			
8	T1	33	7.8	0.139	0.0	LOS A	0.0	0.0	0.00	0.58	82.1			
Approa	ach	253	3.9	0.139	6.9	NA	0.0	0.0	0.00	0.58	54.7			
All Veh	icles	423	3.9	0.139	6.2	NA	0.4	2.9	0.11	0.55	56.5			

igvee Site: Rutherford + Development AM Peak

Proposed Rutherford Road / Development E/W Intersection Giveway / Yield (Two-Way)

Mover	nent Perf	ormance - V	ehicles	;							
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back (Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South:	Rutherford	l Rd									
2	T1	17	7.8	0.011	0.0	LOS A	0.0	0.1	0.04	0.11	95.7
3	R2	3	1.0	0.011	7.5	LOS A	0.0	0.1	0.04	0.11	73.4
Approa	ich	20	6.7	0.011	1.2	NA	0.0	0.1	0.04	0.11	92.1
East: D	evelopme)	nt E/W									
4	L2	11	1.0	0.087	4.6	LOS A	0.3	2.1	0.09	0.54	60.2
6	R2	99	1.0	0.087	4.8	LOS A	0.3	2.1	0.09	0.54	54.2
Approa	ich	109	1.0	0.087	4.7	LOS A	0.3	2.1	0.09	0.54	54.8
North:	Rutherford	Rd									
7	L2	24	1.0	0.019	7.9	LOS A	0.0	0.0	0.00	0.47	39.4
8	T1	11	7.8	0.019	0.0	LOS A	0.0	0.0	0.00	0.47	84.9
Approa	ich	35	3.1	0.019	5.5	NA	0.0	0.0	0.00	0.47	50.7
All Veh	icles	164	2.1	0.087	4.5	NA	0.3	2.1	0.06	0.47	57.8

MOVEMENT SUMMARY

igvee Site: Rutherford + Development PM Peak

Proposed Rutherford Road / Development E/W Intersection Giveway / Yield (Two-Way)

Move	ment Perf	formance - V	/ehicles								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South:	Rutherford	l Rd									
2	T1	20	7.8	0.017	0.2	LOS A	0.1	0.4	0.14	0.21	90.8
3	R2	9	1.0	0.017	7.8	LOS A	0.1	0.4	0.14	0.21	69.7
Appro	ach	29	5.6	0.017	2.6	NA	0.1	0.4	0.14	0.21	84.0
East: [Developmei	nt E/W									
4	L2	4	1.0	0.034	4.7	LOS A	0.1	0.8	0.15	0.54	59.8
6	R2	37	1.0	0.034	5.0	LOS A	0.1	0.8	0.15	0.54	53.8
Appro	ach	41	1.0	0.034	4.9	LOS A	0.1	0.8	0.15	0.54	54.5
North:	Rutherford	Rd									
7	L2	86	1.0	0.065	7.9	LOS A	0.0	0.0	0.00	0.49	39.3
8	T1	33	7.8	0.065	0.0	LOS A	0.0	0.0	0.00	0.49	84.4
Appro	ach	119	2.9	0.065	5.7	NA	0.0	0.0	0.00	0.49	49.4
All Vel	nicles	189	2.9	0.065	5.1	NA	0.1	0.8	0.06	0.46	54.8

✓ Site: Rutherford + Development AM Peak - N/S Blocked

Proposed Rutherford Road / Development E/W Intersection Giveway / Yield (Two-Way)

Move	nent Perf	ormance - V	ehicles/	,							
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South:	Rutherford	Rd									
2	T1	17	7.8	0.011	0.0	LOS A	0.0	0.1	0.05	0.11	95.5
3	R2	3	1.0	0.011	7.6	LOS A	0.0	0.1	0.05	0.11	73.3
Approa	ich	20	6.7	0.011	1.2	NA	0.0	0.1	0.05	0.11	92.0
East: D)evelopme	nt E/W									
4	L2	14	1.0	0.209	4.6	LOS A	0.8	5.6	0.12	0.54	60.0
6	R2	245	1.0	0.209	4.8	LOS A	0.8	5.6	0.12	0.54	54.0
Approa	ich	259	1.0	0.209	4.8	LOS A	0.8	5.6	0.12	0.54	54.4
North:	Rutherford	Rd									
7	L2	43	1.0	0.029	7.9	LOS A	0.0	0.0	0.00	0.54	38.8
8	T1	11	7.8	0.029	0.0	LOS A	0.0	0.0	0.00	0.54	83.1
Approa	ich	54	2.3	0.029	6.3	NA	0.0	0.0	0.00	0.54	45.8
All Veh	icles	333	1.6	0.209	4.8	NA	0.8	5.6	0.10	0.52	54.6

MOVEMENT SUMMARY

▽ Site: Rutherford + Development PM Peak - N/S Blocked

Proposed Rutherford Road / Development E/W Intersection Giveway / Yield (Two-Way)

Move	ment Perl	formance - V	ehicles								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South:	Rutherford		70	V/G	366		VGII			регусп	KIIVII
2	T1	20	7.8	0.017	0.3	LOS A	0.1	0.4	0.19	0.21	90.3
3	R2	9	1.0	0.017	8.0	LOS A	0.1	0.4	0.19	0.21	69.3
Approa	ach	29	5.6	0.017	2.7	NA	0.1	0.4	0.19	0.21	83.5
East: D	Developme	nt E/W									
4	L2	7	1.0	0.059	4.7	LOS A	0.2	1.4	0.17	0.55	59.7
6	R2	62	1.0	0.059	5.1	LOS A	0.2	1.4	0.17	0.55	53.7
Approa	ach	69	1.0	0.059	5.1	LOS A	0.2	1.4	0.17	0.55	54.5
North:	Rutherford	Rd									
7	L2	152	1.0	0.101	7.9	LOS A	0.0	0.0	0.00	0.55	38.7
8	T1	33	7.8	0.101	0.0	LOS A	0.0	0.0	0.00	0.55	82.8
Approa	ach	184	2.2	0.101	6.5	NA	0.0	0.0	0.00	0.55	44.9
All Veh	icles	283	2.3	0.101	5.7	NA	0.2	1.4	0.06	0.51	50.1

▽ Site: Wren + Development AM Peak

Wren Street / Development N/S Intersection Giveway / Yield (Two-Way)

Movement Performance - Vehicles											
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South: Development N/S Rd											
1	L2	75	1.0	0.112	4.7	LOS A	0.4	3.0	0.11	0.53	42.8
3	R2	75	1.0	0.112	5.0	LOS A	0.4	3.0	0.11	0.53	41.6
Approa	ich	149	1.0	0.112	4.8	LOS A	0.4	3.0	0.11	0.53	42.2
East: V	Vren Street	t									
4	L2	19	3.3	0.028	4.6	LOS A	0.0	0.0	0.00	0.19	46.5
5	T1	34	3.3	0.028	0.0	LOS A	0.0	0.0	0.00	0.19	48.0
Approa	ich	53	3.3	0.028	1.7	NA	0.0	0.0	0.00	0.19	47.5
West: \	Wren Stree	t									
11	T1	53	3.3	0.039	0.1	LOS A	0.1	0.8	0.08	0.15	48.2
12	R2	19	3.3	0.039	4.8	LOS A	0.1	0.8	0.08	0.15	45.8
Approa	ich	72	3.3	0.039	1.3	NA	0.1	0.8	0.08	0.15	47.6
All Veh	icles	274	2.0	0.112	3.3	NA	0.4	3.0	0.08	0.36	44.6

MOVEMENT SUMMARY

▽ Site: Wren + Development PM Peak

Wren Street / Development N/S Intersection Giveway / Yield (Two-Way)

Move	ment Perf	ormance - V	ehicles								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South: Development N/S Rd											
1	L2	28	1.0	0.045	4.7	LOS A	0.2	1.1	0.14	0.53	42.7
3	R2	28	1.0	0.045	5.4	LOS A	0.2	1.1	0.14	0.53	41.5
Approa	ach	57	1.0	0.045	5.0	LOS A	0.2	1.1	0.14	0.53	42.1
East: V	Vren Street										
4	L2	65	3.3	0.064	4.6	LOS A	0.0	0.0	0.00	0.30	45.3
5	T1	52	3.3	0.064	0.0	LOS A	0.0	0.0	0.00	0.30	47.0
Approa	ach	117	3.3	0.064	2.6	NA	0.0	0.0	0.00	0.30	46.1
West: V	Wren Stree	t									
11	T1	68	3.3	0.078	0.3	LOS A	0.3	2.4	0.20	0.27	46.5
12	R2	65	3.3	0.078	5.0	LOS A	0.3	2.4	0.20	0.27	44.0
Approa	ach	134	3.3	0.078	2.6	NA	0.3	2.4	0.20	0.27	45.3
All Veh	icles	307	2.9	0.078	3.0	NA	0.3	2.4	0.11	0.33	45.0

▽ Site: Wren + Development AM Peak - E/W Blocked

Wren Street / Development N/S Intersection Giveway / Yield (Two-Way)

Move	ment Perf	formance - V	ehicles								
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/h
South:	Developm	ent N/S Rd									
1	L2	184	1.0	0.182	4.7	LOS A	0.8	5.5	0.11	0.52	42.8
3	R2	75	1.0	0.182	5.2	LOS A	0.8	5.5	0.11	0.52	41.7
Approa	ach	259	1.0	0.182	4.8	LOS A	0.8	5.5	0.11	0.52	42.5
East: V	Vren St										
4	L2	19	3.3	0.028	4.6	LOS A	0.0	0.0	0.00	0.19	46.5
5	T1	34	3.3	0.028	0.0	LOS A	0.0	0.0	0.00	0.19	48.0
Approa	ach	53	3.3	0.028	1.7	NA	0.0	0.0	0.00	0.19	47.5
West:	Wren Stree	t									
11	T1	53	3.3	0.054	0.1	LOS A	0.2	1.5	0.12	0.24	47.0
12	R2	43	3.3	0.054	4.8	LOS A	0.2	1.5	0.12	0.24	44.6
Approa	ach	96	3.3	0.054	2.2	NA	0.2	1.5	0.12	0.24	46.0
All Veh	icles	407	1.8	0.182	3.8	NA	0.8	5.5	0.10	0.41	44.0

MOVEMENT SUMMARY

▽ Site: Wren + Development PM Peak - E/W Blocked

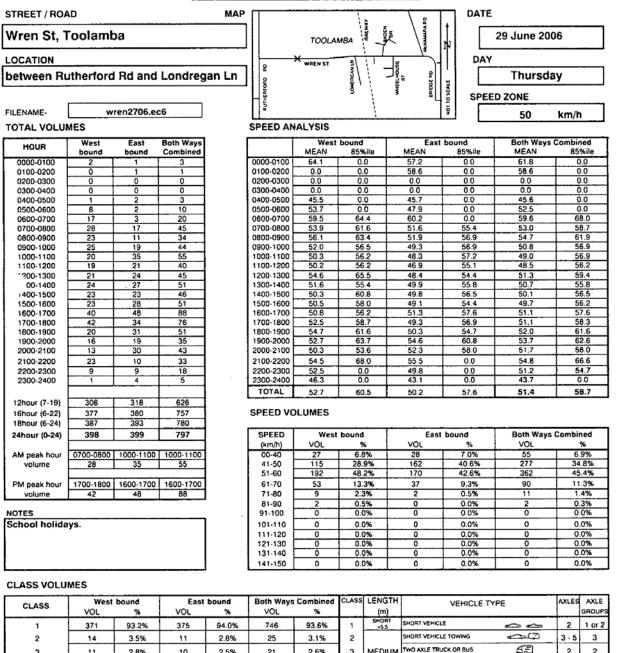
Wren Street / Development N/S Intersection Giveway / Yield (Two-Way)

Move	ment Perf	ormance - V	ehicles/	,							,
Mov ID	OD Mov	Demand Total veh/h	Flows HV %	Deg. Satn v/c	Average Delay sec	Level of Service	95% Back Vehicles veh	of Queue Distance m	Prop. Queued	Effective Stop Rate per veh	Average Speed km/t
South:	Developme	ent N/S Rd		110	000		Von			porton	
1	L2	76	1.0	0.078	4.7	LOS A	0.3	2.1	0.12	0.52	42.7
3	R2	28	1.0	0.078	5.8	LOS A	0.3	2.1	0.12	0.52	41.6
Approa	ach	104	1.0	0.078	5.0	LOS A	0.3	2.1	0.12	0.52	42.4
East: V	Vren St										
4	L2	65	3.3	0.064	4.6	LOS A	0.0	0.0	0.00	0.30	45.3
5	T1	52	3.3	0.064	0.0	LOS A	0.0	0.0	0.00	0.30	47.0
Approa	ach	117	3.3	0.064	2.6	NA	0.0	0.0	0.00	0.30	46.1
West:	Wren Stree	t									
11	T1	68	3.3	0.133	0.4	LOS A	0.7	4.7	0.24	0.37	45.4
12	R2	152	3.3	0.133	5.0	LOS A	0.7	4.7	0.24	0.37	42.9
Approa	ach	220	3.3	0.133	3.6	NA	0.7	4.7	0.24	0.37	43.7
All Veh	icles	441	2.8	0.133	3.6	NA	0.7	4.7	0.15	0.39	44.0

APPENDIX C Traffic Counts

CITY OF GREATER SHEPPARTON

SINGLE DAY TRAFFIC COUNT SUMMARY



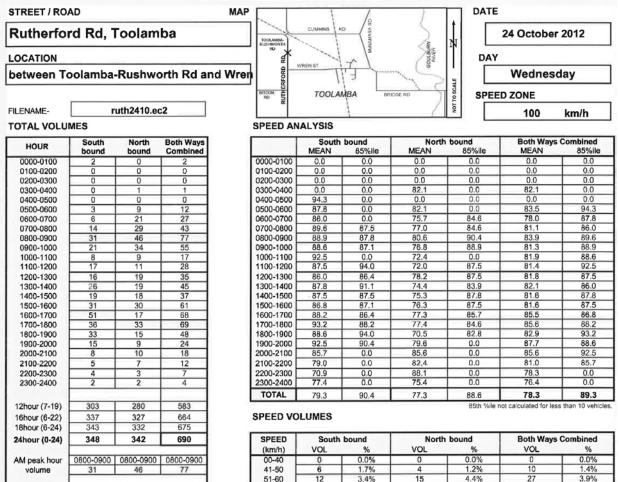
	VOL	%	VOL	%	VOL	%		(m)	
1	371	93.2%	375	94.0%	746	93.6%	1	SHORT <5.5	SHORT VEHICLE
2	14	3.5%	11	2.8%	25	3.1%	2		SHORT VEHICLE TOWING
3	11	2.8%	10	2.5%	21	2.6%	3	MEDIUM	TWO AXLE TRUCK OR BU
4	0	0.0%	1	0.3%	1	0.1%	4	6.5 - 14.5	THREE AXLE TRUCK OR
5	1	0.3%	1	0.3%	2	0.3%	5		FOUR AXLE TRUCK
6	0	0.0%	0	0.0%	0	0.0%	6		3 AXLE ARTICULATED VE
7	0	0.0%	1	0.3%	1	0.1%	7	LONG	4 AXLE ARTICULATED VE
8	1	0.3%	0	0.0%	1	0.1%	8	11.5 - 19.0	5 AXLE ARTICULATED VE
9	0	0.0%	0	0.0%	0	0.0%	9		6 AXLE ARTICULATED VE
10	0	0.0%	0	0.0%	0	0.0%	10	MEDIUM	8-DOUBLE
11	0	0.0%	0	0.0%	0	0.0%	11		DOUBLE ROAD TRAIN
12	0	0.0%	0	0.0%	0	0.0%	12	>33.0	TRIPLE ROAD TRAIN
13	0	0.0%	0	0.0%	0	0.0%	13		ALL OTHER VEHICLES
								For fur	ther information, ple
Commercial (Class 3-12)	13	3.3%	13	3.3%	26	3.3%			at Locked Bag 100

	(m)				GROUPS
1	SHORT	SHORT VEHICLE		2	1 or 2
2		SHORT VEHICLE TOWING		3 - 5	3
3	MEDIUM	TWO AXLE TRUCK OR BUS	53	2	2
4	6.5 - 14.5	THREE AXLE TRUCK OR BUS	Carrier and	3	2
5		FOUR AXLE TRUCK	観幻	>3	2
6		3 AXLE ARTICULATED VEHICLE	filler	3	3
7	LONG	4 AXLE ARTICULATED VEHICLE		4	>2
в	11.5 - 19.0	S AXLE ARTICULATED VEHICLE	E como	5	>2
9		6 AXLE ARTICULATED VEHICLE	6-000	>5	>2
0	MEDIUM	8-DOUBLE	0.00 000 000	>6	4
1	17.5-36.5	DOUBLE ROAD TRAIN	Comer Comert	>6	5 or 6
2	>33.0	TRIPLE ROAD TRAIN		>6	>6
3		ALL OTHER VEHICLES			

further information, please contact Design Services at Locked Bag 1000, Shepparton 3632.

CITY OF GREATER SHEPPARTON

SINGLE DAY TRAFFIC COUNT SUMMARY



NOTES

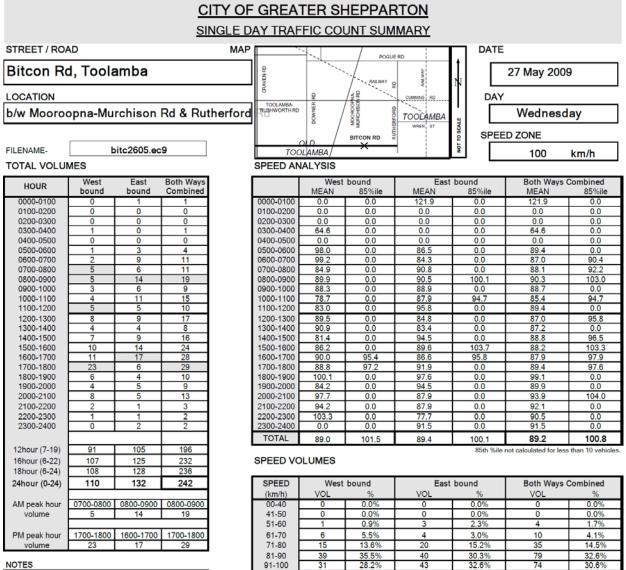
PM peak hour volume

1600-1700 1700-1800 1700-1800 51 33 69

51-60	12	3.4%	15	4.4%	27	3.9%
61-70	50	14.4%	66	19.3%	116	16.8%
71-80	102	29.3%	113	33.0%	215	31.2%
81-90	123	35.3%	100	29.2%	223	32.3%
91-100	42	12.1%	36	10.5%	78	11.3%
101-110	12	3.4%	8	2.3%	20	2.9%
111-120	1	0.3%	0	0.0%	1	0.1%
121-130	0	0.0%	0	0.0%	0	0.0%
131-140	0	0.0%	0	0.0%	0	0.0%
141-150	0	0.0%	0	0.0%	0	0.0%

CLASS VOLUMES

CLASS	South VOL	bound %	North VOL	bound %	Both Way VOL	s Combined %	CLASS	LENGTH (m)	VEHICLE T	E TYPE		AXLE GROUP
1	310	89.1%	310	90.6%	620	89.9%	1	SHORT <5.5	SHORT VEHICLE		2	1 or 2
2	11	3.2%	5	1.5%	16	2.3%	2		SHORT VEHICLE TOWING		3 - 5	3
3	23	6.6%	23	6.7%	46	6.7%	3	MEDIUM	TWO AXLE TRUCK OR BUS	5E	2	2
4	3	0.9%	2	0.6%	5	0.7%	4	6.5 - 14.5	THREE AXLE TRUCK OR BUS	Contraction of the second	3	2
5	0	0.0%	1	0.3%	1	0.1%	5		FOUR AXLE TRUCK	5000	>3	2
6	1	0.3%	1	0.3%	2	0.3%	6		3 AXLE ARTICULATED VEHICLE	Els	3	3
7	0	0.0%	0	0.0%	0	0.0%	7	LONG	4 AXLE ARTICULATED VEHICLE	60000	4	>2
8	0	0.0%	0	0.0%	0	0.0%	8	11.5 - 19.0	5 AXLE ARTICULATED VEHICLE	6 00 00	5	>2
9	0	0.0%	0	0.0%	0	0.0%	9		6 AXLE ARTICULATED VEHICLE	000-100	>5	>2
10	0	0.0%	0	0.0%	0	0.0%	10		B-DOUBLE	00 000 000	>6	4
11	0	0.0%	0	0.0%	0	0.0%	11	17.5-36.5	DOUBLE ROAD TRAIN	6-201-000 001-000	>6	5 or 6
12	0	0.0%	0	0.0%	0	0.0%	12	>33.0	TRIPLE ROAD TRAIN		>6	>6
13	0	0.0%	0	0.0%	0	0.0%	13	-	ALL OTHER VEHICLES			- 1940
							For further information, please contact Design Services					
Commercial (Class 3-12)	27	7.8%	27	7.9%	54	7.8%						



Ν	0	Т	E	s	

SPEED	West	bound	East	bound	Both Ways (Combined
(km/h)	VOL	%	VOL	%	VOL	%
00-40	0	0.0%	0	0.0%	0	0.0%
41-50	0	0.0%	0	0.0%	0	0.0%
51-60	1	0.9%	3	2.3%	4	1.7%
61-70	6	5.5%	4	3.0%	10	4.1%
71-80	15	13.6%	20	15.2%	35	14.5%
81-90	39	35.5%	40	30.3%	79	32.6%
91-100	31	28.2%	43	32.6%	74	30.6%
101-110	13	11.8%	18	13.6%	31	12.8%
111-120	4	3.6%	2	1.5%	6	2.5%
121-130	0	0.0%	2	1.5%	2	0.8%
131-140	0	0.0%	0	0.0%	0	0.0%
141-150	1	0.9%	0	0.0%	1	0.4%

CLASS VOLUMES

CLASS	West VOL	bound %	East VOL	bound %	Both Ways VOL	Combined %	CLASS	LENGTH (m)	VEHICLE T	YPE	AXLES	AXLE GROUPS
1	97	88.2%	115	87.1%	212	87.6%	1	011007	SHORT VEHICLE	<u>്</u> ം	2	1 or 2
2	6	5.5%	8	6.1%	14	5.8%	2		SHORT VEHICLE TOWING		3-5	3
3	6	5.5%	9	6.8%	15	6.2%	3	MEDIUM	TWO AXLE TRUCK OR BUS	ধান্থা	2	2
4	0	0.0%	0	0.0%	0	0.0%	4	6.5 - 14.5	THREE AXLE TRUCK OR BUS	00000	3	2
5	0	0.0%	0	0.0%	0	0.0%	5		FOUR AXLE TRUCK	00000	>3	2
6	0	0.0%	0	0.0%	0	0.0%	6		3 AXLE ARTICULATED VEHICLE	00000	3	3
7	0	0.0%	0	0.0%	0	0.0%	7	LONG	4 AXLE ARTICULATED VEHICLE	00000	4	>2
8	1	0.9%	0	0.0%	1	0.4%	8	11.5 - 19.0	5 AXLE ARTICULATED VEHICLE	00 00	5	>2
9	0	0.0%	0	0.0%	0	0.0%	9		6 AXLE ARTICULATED VEHICLE	0 001-000	>5	>2
10	0	0.0%	0	0.0%	0	0.0%	10	MEDIUM COMBINATION	B-DOUBLE	0 00 000 000	>6	4
11	0	0.0%	0	0.0%	0	0.0%	11	17.5-36.5	DOUBLE ROAD TRAIN	6-007-000 007-000	>6	5 or 6
12	0	0.0%	0	0.0%	0	0.0%	12	>33.0	TRIPLE ROAD TRAIN	Concertor concertor	>6	>6
13	0	0.0%	0	0.0%	0	0.0%	13	-	ALL OTHER VEHICLES		-	-
						For further information, please contact Design Services						
Commercial (Class 3-12)	7	6.4%	9	6.8%	16	6.6%	at Locked Bag 1000, Shepparton 3632.					

CITY OF GREATER SHEPPARTON

SINGLE DAY TRAFFIC COUNT SUMMARY

ren	amba n St prid1812.e North bound 1 0 0 1 2 7 1 6 17 14 14 15 18 13 31 21 12 11 11 13	Both Ways Combined 1 0 0 2 2 3 4 1 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		SPEED A SPEED A SPEED A SPEED A SPEED A SOULD SUBJECT SPEED A SPEED A	Sout MEAN 0.0 0.0 74.0 76.1 73.9 70.0 74.0 72.4 71.1 71.2 68.1 68.9 72.7 72.7		5%ile 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	North MEAN 67.8 0.0 51.5 67.5 68.2 68.2 68.2 66.3 64.9 69.2 64.9	N DA' DA' DA' SPE SPE SPE SPE SPE SPE SPE SPE SPE SPE	Wednesd ED ZONE 50 Both Ways MEAN 67.8 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	km/	/h
br	North bound 1 0 0 1 2 7 16 17 14 14 14 14 14 13 13 13 31 21 41 19 12 11	Both Ways Combined 1 0 0 2 3 4 1 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		0000-0100 0100-0200 0200-0300 0300-0400 0500-0600 0500-0600 0500-0900 0500-0900 0500-1000 1000-1100 1100-1200 1200-1300 1300-1400 1400-1500 1600-1700	NALYSIS Sout MEAN 0.0 0.0 0.0 74.2 74.7		5%ile 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	North MEAN 67.8 0.0 0.0 51.5 67.5 75.0 68.2 62.7 65.6 66.3 64.9 60.2	bound 85%ile 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	Wednesd ED ZONE 50 Both Ways MEAN 67.8 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	km/	Ined 5%ile 0.0 0.0 0.0 0.0 0.0 85.3 79.6 82.1 77.8
br	North bound 1 0 0 1 2 7 16 17 14 14 14 14 14 13 13 13 31 21 41 19 12 11	Both Ways Combined 1 0 0 2 3 4 1 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		0000-0100 0100-0200 0200-0300 0300-0400 0500-0600 0500-0600 0500-0900 0500-0900 0500-1000 1000-1100 1100-1200 1200-1300 1300-1400 1400-1500 1600-1700	NALYSIS Sout MEAN 0.0 0.0 0.0 74.2 74.7		5%ile 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	North MEAN 67.8 0.0 0.0 51.5 67.5 75.0 68.2 62.7 65.6 66.3 64.9 60.2	bound 85%ile 0.0 0.0 0.0 0.0 0.0 0.0 0.0 79.9 67.7 74.5 76.2 0.0 77.8	ED ZONE 50 Both Ways MEAN 67.8 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	km/	Ined 5%ile 0.0 0.0 0.0 0.0 0.0 0.0 85.3 79.6 82.1 77.8
	North bound 1 0 0 1 2 7 16 17 14 14 14 14 14 13 13 13 13 13 13 12 11	Both Ways Combined 1 0 0 2 3 4 1 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		0000-0100 0100-0200 0200-0300 0300-0400 0500-0600 0500-0600 0500-0900 0500-0900 0500-1000 1000-1100 1100-1200 1200-1300 1300-1400 1400-1500 1600-1700	Sout MEAN 0.0 0.0 74.0 76.1 73.9 70.0 74.0 72.4 71.1 71.2 68.1 68.9 72.7 72.7		5%ile 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	North MEAN 67.8 0.0 0.0 51.5 67.5 75.0 68.2 62.7 65.6 66.3 64.9 69.2	bound 85%ile 0.0 0.0 0.0 0.0 0.0 0.0 0.0 79.9 67.7 74.5 76.2 0.0 77.8	50 Both Ways MEAN 67.8 0.0 0.0 0.0 62.8 74.2 74.2 74.2 69.3 69.4 68.9 68.0 69.7 68.7	Comb	Ined 5%ile 0.0 0.0 0.0 0.0 0.0 0.0 85.3 79.6 82.1 77.8
	North bound 1 0 0 1 2 7 16 17 14 14 14 14 14 13 13 13 13 13 13 12 11	Both Ways Combined 1 0 0 2 3 4 1 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		0000-0100 0100-0200 0200-0300 0300-0400 0500-0600 0500-0600 0500-0900 0500-0900 0500-1000 1000-1100 1100-1200 1200-1300 1300-1400 1400-1500 1600-1700	Sout MEAN 0.0 0.0 74.0 76.1 73.9 70.0 74.0 72.4 71.1 71.2 68.1 68.9 72.7 72.7		5%ile 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	North MEAN 67.8 0.0 0.0 51.5 67.5 75.0 68.2 62.7 65.6 66.3 64.9 69.2	bound 85%ile 0.0 0.0 0.0 0.0 0.0 0.0 0.0 79.9 67.7 74.5 76.2 0.0 77.8	Both Ways MEAN 67.8 0.0 0.0 62.8 74.2 74.2 69.3 69.4 68.9 68.0 69.7 68.7	Comb	Ined 5%ile 0.0 0.0 0.0 0.0 0.0 85.3 79.6 82.1 77.8
	bound 1 0 0 1 2 7 16 17 14 14 13 13 31 21 41 19 12 11	Combined 1 0 0 2 3 23 41 42 27 22 21 32 20 34 49 51 65 28 20 24		0000-0100 0100-0200 0200-0300 0300-0400 0500-0600 0500-0600 0500-0900 0500-0900 0500-1000 1000-1100 1100-1200 1200-1300 1300-1400 1400-1500 1600-1700	Sout MEAN 0.0 0.0 74.0 76.1 73.9 70.0 74.0 72.4 71.1 71.2 68.1 68.9 72.7 72.7		5%ile 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	MEAN 67.8 0.0 0.0 51.5 67.5 75.0 68.2 62.7 65.6 66.3 66.3 64.9 69.2	85%le 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 79.9 67.7 74.5 75.2 0.0 77.8	MEAN 67.8 0.0 0.0 62.8 74.2 69.3 69.4 68.9 68.0 69.7 68.7		5%ile 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 85.3 79.6 82.1 77.8
	bound 1 0 0 1 2 7 16 17 14 14 13 13 31 21 41 19 12 11	Combined 1 0 0 2 3 23 41 42 27 22 21 32 20 34 49 51 65 28 20 24		0100-0200 0200-0300 0300-0400 0500-0600 0500-0600 0700-0800 0800-0700 0800-1000 1100-1200 1200-1300 1300-1400 1400-1500 1500-1600 1600-1700	MEAN 0.0 0.0 74.0 76.1 73.9 70.0 74.0 74.0 74.0 74.0 74.0 72.4 71.1 71.2 68.1 68.9 72.7 72.7		5%ile 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	MEAN 67.8 0.0 0.0 51.5 67.5 75.0 68.2 62.7 65.6 66.3 66.3 64.9 69.2	85%le 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 79.9 67.7 74.5 75.2 0.0 77.8	MEAN 67.8 0.0 0.0 62.8 74.2 69.3 69.4 68.9 68.0 69.7 68.7		5%ile 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 85.3 79.6 82.1 77.8
	0 0 1 2 7 16 17 14 14 14 5 18 13 13 13 13 13 13 13 13 12 12 11	0 0 2 9 23 41 42 27 22 21 32 20 34 49 51 65 26 20 24		0100-0200 0200-0300 0300-0400 0500-0600 0500-0600 0700-0800 0800-0700 0800-1000 1100-1200 1200-1300 1300-1400 1400-1500 1500-1600 1600-1700	0.0 0.0 74.0 76.1 73.9 70.0 74.0 72.4 71.1 71.2 68.1 68.9 72.7 72.7		0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 51.5 67.5 75.0 68.2 62.7 65.6 66.3 64.9 69.2	0.0 0.0 0.0 0.0 79.9 67.7 74.5 75.2 0.0 77.8	0.0 0.0 62.8 74.2 74.2 69.3 69.4 68.9 68.0 69.7 68.7		0.0 0.0 0.0 0.0 85.3 79.6 82.1 77.8
	0 1 2 7 16 17 14 14 14 14 14 13 13 13 13 13 21 21 21 21 21 21	0 2 9 23 41 42 27 22 21 21 20 34 49 51 65 20 24		0300-0400 0400-0500 0500-0600 0600-0700 0700-0800 0800-0900 0900-1000 1100-1100 1200-1300 1300-1400 1500-1600 1600-1700	0.0 74.0 76.1 73.9 70.0 72.4 71.1 71.2 68.1 68.9 72.7 72.7		0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 51.5 67.5 75.0 68.2 62.7 65.6 66.3 64.9 69.2	0.0 0.0 79.9 67.7 74.5 75.2 0.0 77.8	0.0 62.8 74.2 69.3 69.4 68.9 68.0 68.0 69.7 68.7		0.0 0.0 85.3 79.6 82.1 77.8
	1 2 7 16 17 14 14 5 18 13 13 13 13 21 21 12 11	2 9 23 41 42 27 22 21 20 34 49 51 65 28 20 20 24		0400-0500 0500-0600 0700-0800 0900-0900 0900-1000 1100-1100 1100-1200 1200-1300 1300-1400 1500-1600 1600-1700	74.0 76.1 73.9 70.0 74.0 72.4 71.1 71.2 68.1 68.9 72.7 72.7		0.0 0.0 35.3 78.5 32.1 32.1 0.0 76.7 78.8	51.5 67.5 75.0 68.2 62.7 65.6 66.3 64.9 69.2	0.0 0.0 79.9 67.7 74.5 75.2 0.0 77.8	62.8 74.2 69.3 69.4 68.9 68.0 68.0 68.7		0.0 0.0 85.3 79.6 82.1 77.8
	2 7 16 17 14 14 5 18 13 13 13 13 13 13 21 21 41 19 12 11	9 23 41 42 27 22 21 32 20 34 49 51 65 26 20 20 24		0500-0600 0600-0700 0700-0800 0900-1000 1000-1100 1100-1200 1200-1300 1400-1500 1500-1600 1600-1700	76.1 73.9 70.0 72.4 71.1 71.2 68.1 68.9 72.7 72.7		0.0 35.3 78.5 32.1 32.1 0.0 76.7 78.8	67.5 75.0 68.2 62.7 65.6 66.3 64.9 69.2	0.0 0.0 79.9 67.7 74.5 75.2 0.0 77.8	74.2 74.2 69.3 69.4 68.9 68.0 68.0 68.7		0.0 85.3 79.6 82.1 77.8
	16 17 14 14 5 18 13 13 31 21 21 19 12 11	41 27 22 21 32 20 34 49 51 65 28 20 20 24		0600-0700 0700-0800 0800-0900 0900-1000 1000-1100 1200-1300 1300-1400 1400-1500 1500-1500 1600-1700	73.9 70.0 74.0 72.4 71.1 71.2 68.1 68.9 72.7 72.7		35.3 78.5 32.1 32.1 0.0 76.7 78.8	75.0 68.2 62.7 65.6 66.3 64.9 69.2	0.0 79.9 67.7 74.5 75.2 0.0 77.8	74.2 69.3 69.4 68.9 68.0 69.7 68.7		85.3 79.6 82.1 77.8
	17 14 14 5 18 13 13 31 21 41 19 12 11	42 27 22 21 32 20 34 49 51 65 26 20 20 24		0800-0900 0900-1000 1000-1100 1200-1200 1200-1300 1300-1400 1400-1500 1500-1600 1600-1700	74.0 72.4 71.1 68.1 68.9 72.7 72.7		32.1 32.1 0.0 76.7 78.8	62.7 65.6 66.3 64.9 69.2	67.7 74.5 75.2 0.0 77.8	69.4 68.9 68.0 69.7 68.7		82.1 77.8
	14 14 5 18 13 13 31 21 41 19 12 11	27 22 21 32 20 34 49 51 65 28 20 20 24		0900-1000 1000-1100 1100-1200 1200-1300 1300-1400 1400-1500 1500-1600 1600-1700	72.4 71.1 68.1 68.9 72.7 72.7		32.1 0.0 76.7 78.8	65.6 66.3 64.9 69.2	74.5 75.2 0.0 77.8	68.9 68.0 69.7 68.7		77.8
	14 5 18 13 13 31 21 41 19 12 11	22 21 32 20 34 49 51 65 26 20 20 24		1000-1100 1100-1200 1200-1300 1300-1400 1400-1500 1500-1600 1600-1700	71.1 71.2 68.1 68.9 72.7 72.7		0.0 76.7 78.8	66.3 64.9 69.2	75.2 0.0 77.8	68.0 69.7 68.7		
	5 18 13 31 21 41 19 12 11	21 32 20 34 49 51 65 26 20 20 24		1100-1200 1200-1300 1300-1400 1400-1500 1500-1600 1600-1700	71.2 68.1 68.9 72.7 72.7		76.7 78.8	64.9 69.2	0.0 77.8	69.7 68.7		
	13 13 31 21 41 19 12 11	20 34 49 51 65 26 20 20 24		1300-1400 1400-1500 1500-1600 1600-1700	68.9 72.7 72.7							76.7
	13 31 21 41 19 12 11	34 49 51 65 26 20 20 24		1400-1500 1500-1600 1600-1700	72.7 72.7		0.0	64.0	72.4	1 00.0		78.8
	31 21 41 19 12 11	49 51 65 26 20 20 24		1500-1600 1600-1700	72.7	<u> </u>	0.0			66.3		74.2
	21 19 12 11	51 65 26 20 24		1600-1700			32.1 79.2	63.8 64.5	69.5 74.9	69.3 67.5		79.9 76.7
	41 19 12 11	65 26 20 24			72.0		31.7	66.2	79.2	69.6		80.6
-	12 11	20 24		1700-1800	66.6		7.8	66.2	74.9	66.3	i	76.7
	11	24		1800-1900	71.3		0.0	63.0	69.1	65.2		72.4
+				1900-2000 2000-2100	68.1 70.1		0.0 78.5	61.9 61.2	69.1 65.9	64.4 66.0		77.0 73.4
+		1 24	1	2100-2200	67.9		5.2	63.2	72.4	65.4		74.9
	8	13	1	2200-2300	79.1		0.0	77.1	0.0	77.9		79.6
	1	2		2300-2400	67.3		0.0	69.7	0.0	68,5		0.0
				TOTAL	71.2	1 8	1.7	65.6	75.2	68.4		79.2
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+	274	536		SPEED	Cauth	ı boun	. 1997 (* 19	North		Both Ways	Cambl	1991 A
	210	040		(km/h)	VOL	i Douii	%	VOL	800110 %	VOL		%
0 0	0800-0900	0800-0900		00-40	3	1	.1%	4	1.4%	7		.3%
	17	42		41-50	8		.0%	14	5.0%	22	4	.0%
		1		51-60	28).4%	63	22.7%	91		6.6%
10 1	1700-1800	1700-1800 65		61-70	66		.4%	109	39.2%	175		1.9%
	41	65		71-80 81-90	109 47		.4%	69 18	24.8%	178 65		2.5% 1.9%
				91-100	-47		.0%	0	0.0%	8		.5%
2 98	C C AN CONTRACT			101-110	1		4%	0	0.0%	1		.2%
				111-120	0	-	.0%	0	0.0%	0	-	.0%
				121-130	0	0	.0%	0	0.0%	0	0	.0%
				131-140	0	0	.0%	1	0.4%	1	0	.2%
12				141-150	0	0	.0%	0	0.0%	0		.0%
th bo	bound	North	bound	Both Ways	Combined	CLASS	LENGTH		VEHICLE TY	/PF	AXLES	AXL
	%	VOL	%	VOL	%	10.53	(m)				in in the second	GROU
	91.5%	252	90.6%	499	91.1%		SHORT <5.5	SHORT VEHICLE		هيه ه يه	2	1 or
	7.0%	18	6.5%	37	6.8%	2		SHORT VEHICLE	TOWING	¢ no la	3 - 5	3
	1.5%	8	2.9%	12	2.2%	3	MEDIUM	TWO AXLE TRUC	K OR BUS	(IE)	2	2
	0.0%	0	0.0%	0	0.0%	4	6.5 - 14.5	THREE AXLE TR	JCK OR BUS	62.00	3	2
	0.0%	0	0.0%	0	0.0%	5		FOUR AXLE TRU	CK	650	>3	2
				1 1		100.0	├ ──			A CON		
						100000						3
						1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.						>2
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		0	0.0%	0	0.0%	10	MEDIUM	8-DOUBLE			>6	4
	0.0%	0	0.0%	0	0.0%	A DECEMBER OF THE OWNER		DOUBLE ROAD T	RAIN		>8	5 or
	0.0%					the Second Constants		TRIPLE ROAD TR	AIN			>6
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		0.0% 0.0% 0.0% 0.0%	0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0	0.0% 0 0.0% 0.0% 0 0.0% 0.0% 0 0.0% 0.0% 0 0.0% 0.0% 0 0.0% 0.0% 0 0.0% 0.0% 0 0.0% 0.0% 0 0.0% 0.0% 0 0.0%	0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0 0.0% 0	0.0% 0 0.0% 0 0.0% 0.0% 0 0.0% 0 0.0% 0.0% 0 0.0% 0 0.0% 0.0% 0 0.0% 0 0.0% 0.0% 0 0.0% 0 0.0% 0.0% 0 0.0% 0 0.0% 0.0% 0 0.0% 0 0.0% 0.0% 0 0.0% 0 0.0%	0.0% 0 0.0% 0 0.0% 7 0.0% 0 0.0% 0 0.0% 8 0.0% 0 0.0% 0 0.0% 8 0.0% 0 0.0% 0 0.0% 9 0.0% 0 0.0% 0 0.0% 10 0.0% 0 0.0% 0 0.0% 11 0.0% 0 0.0% 0 0.0% 12 0.0% 0 0.0% 0 0.0% 13	0.0% 0 0.0% 0 0.0% 7 LONG 0.0% 0 0.0% 0 0.0% 8 11.5 - 19.0 0.0% 0 0.0% 0 0.0% 9 11.5 - 19.0 0.0% 0 0.0% 0 0.0% 10 MEDIUM COMEINATION 0.0% 0 0.0% 0 0.0% 11 17.6 - 36.5 0.0% 0 0.0% 0 0.0% 12 >33.0 0.0% 0 0.0% 0 0.0% 13 -	0.0% 0 0.0% 0 0.0% 7 LONG 4AXLE ARTICUL/ 0.0% 0 0.0% 0 0.0% 7 LONG 4AXLE ARTICUL/ 0.0% 0 0.0% 0 0.0% 8 11.5 - 19.0 5AXLE ARTICUL/ 0.0% 0 0.0% 0 0.0% 9 MEDIUM 6AXLE ARTICUL/ 0.0% 0 0.0% 0 0.0% 10 Communication BOUBLE 0.0% 0 0.0% 0 0.0% 11 17.6 36.5 DOUBLE ROAD TR 0.0% 0 0.0% 0 0.0% 12 >33.0 TRPLE ROAD TR 0.0% 0 0.0% 0 0.0% 13 - ALL OTHER VERS	0.0% 0 0.0% 0 0.0% 7 LONG 4 AXLE ARTICULATED VENCLE 0.0% 0 0.0% 0 0.0% 8 11.5 - 19.0 5 AXLE ARTICULATED VENCLE 0.0% 0 0.0% 0 0.0% 9 11.5 - 19.0 5 AXLE ARTICULATED VENCLE 0.0% 0 0.0% 0 0.0% 9 MEDIUM 5 AXLE ARTICULATED VENCLE 0.0% 0 0.0% 0 0.0% 10 MEDIUM 5 AXLE ARTICULATED VENCLE 0.0% 0 0.0% 0 0.0% 10 MEDIUM 5 AXLE ARTICULATED VENCLE 0.0% 0 0.0% 0 0.0% 11 17.5 - 36.6 DOUBLE ROAD TRAIN 0.0% 0 0.0% 0 0.0% 12 >33.0 TRIPLE ROAD TRAIN 0.0% 0 0.0% 0 0.0% 13 - ALL OTHER VENCLES	0.0% 0 0.0% 0 0.0% 7 LONG 4 XUE ARTICULATED VEHICLE 4 XUE ARTICULATED VEHICLE <td>0.0% 0 0.0% 0 0.0% 7 LONG 4 XLE ARTICULATED VEHICLE 4 0.0% 0 0.0% 0 0.0% 8 11.5 - 19.0 5 AXLE ARTICULATED VEHICLE 5 5 5 0.0% 0 0.0% 0 0.0% 9 6 AXLE ARTICULATED VEHICLE 5 5 5 0.0% 0 0.0% 0 0.0% 9 6 AXLE ARTICULATED VEHICLE 5 5 5 0.0% 0 0.0% 0 0.0% 10 6 MEDIUM Commentariant 6 DOUBLE 6 5 5 5 0.0% 0 0.0% 0 0.0% 11 17.5 -36.5 DOUBLE ROAD TRAIN 5 5 5 5 5 5 6 5 <</td>	0.0% 0 0.0% 0 0.0% 7 LONG 4 XLE ARTICULATED VEHICLE 4 0.0% 0 0.0% 0 0.0% 8 11.5 - 19.0 5 AXLE ARTICULATED VEHICLE 5 5 5 0.0% 0 0.0% 0 0.0% 9 6 AXLE ARTICULATED VEHICLE 5 5 5 0.0% 0 0.0% 0 0.0% 9 6 AXLE ARTICULATED VEHICLE 5 5 5 0.0% 0 0.0% 0 0.0% 10 6 MEDIUM Commentariant 6 DOUBLE 6 5 5 5 0.0% 0 0.0% 0 0.0% 11 17.5 -36.5 DOUBLE ROAD TRAIN 5 5 5 5 5 5 6 5 <

APPENDIX D Proposed Pedestrians and Cyclists Facilities

Toolamba Circuit

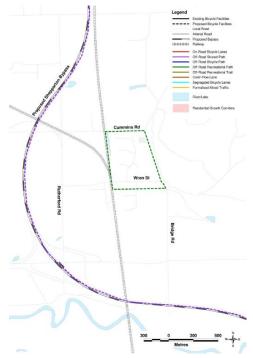


Tatura – Toolamba Circuit



Proposed Toolamba Facilities

Opportunity to provide a 2.6km recreational loop that also accesses the local school and sports grounds.



Proposed Toolamba Walking Track



APPENDIX E VLimits Report IndividualReport VLimits 3.0 Project Report

Suggested Speed Limit:





Rutherford Road Location:South of Wren Street Intersection Suburb / place:Toolamba Local government:SHEPPARTON VicRoads Region:VicRoads - Kew Analysed by:Uwe Paffrath User reference:Residential Development, Rev.1 Review date:4/06/2015

Additional issues to be considered

The measured 85th %ile speed of 90 km/h is significantly higher than the suggested speed limit of 50 km/h. This represents a significant difference between the current behaviour of drivers and the suggested limit. Further investigation should be undertaken to determine the reason for this discrepancy.

A lower speed limit may be appropriate due to the following factors: recreational or tourist traffic. access to Goulburn River The road infrastructure factor(s) listed below may be contributing to the increased risk of crashes. Where crash rates are high and options to improve the road deficiencies have been exhausted, or are not feasible in the short term, a reduced speed limit may be appropriate.

narrow or unsealed shoulders (rural roads only).

Development type

Partially built-up

85th %ile speed

The 85th %ile speed is 90 km/h.

Road characteristics

Length of the section of road is 0.92 km.

The AADT on this road is 1500 vpd.

The existing posted speed limit on the section of road is 100 km/h.

Frequency of roadside accesses

	Type of access	Number
A	Residences, small commercial establishments, small public buildings and other units which generate light and/or occasional activity. (The weighting for this type of access is 1).	11
В	 Average commercial establishment, schools, caravan parks, light industries, public buildings and units generating activity which is either: 1. continuous light 2. moderate at certain times, such as commuting hours 3. substantial at infrequent intervals (The weighting for this type of access is 2). 	0
с	Heavy industry, schools, small shopping centres, petrol stations and other units generating continuous moderate activity or substantial activity at certain regular times. (The weighting for this type of access is 3).	0
D	Large shopping centres and other units generating substantial and continuous activity. Some large industries which are tourist attractions or for some other reason generate substantial traffic volumes would be included in this activity. (The weighting for this type of access is 4).	0

	per 100 m	1.00
Н	Roundabouts, signalised intersecting roads and any at-grade rail crossings. (The weighting for this type of access is 3). Average number of accesses	0
G	Unsignalised intersecting roads (including service road connections) of comparable or greater significance than the road being assessed. Intersections which have a pronounced effect on the traffic flow pattern of the road being considered. (The weighting for this type of access is 3).	2
F	Unsignalised intersecting roads (including service road connections) of lesser importance than the road being assessed but where the side road traffic and turning movements are such that the intersection has an appreciable effect on the traffic flow pattern of the road being considered. (The weighting for this type of access is 2).	0
E	Unsignalised intersecting roads (including service road connections) of substantially lesser importance than the road being assessed, or intersecting roads where side traffic and turning movements have little effect on the traffic flow pattern of the road being considered. (The weighting for this type of access is 1).	0

Divided/undivided The road is **undivided**. Road function The road's function is **collector**. Adjacent speed zones

Approach 1: 100 km/h - southern approach Approach 2: 100 km/h - northern approach